



**Methods for Homogenization of Spatio-Temporal  $B_0$  Magnetic Field  
Variations in Cardiac MRI at Ultra-High Field Strength**

**Methoden zur Homogenisierung räumlicher und zeitlicher Variationen  
des  $B_0$ -Feldes in der kardialen Ultrahochfeld-MRT**

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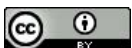
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## Summary

Cardiovascular disease is one of the leading causes of death worldwide and, so far, echocardiography, nuclear cardiology, and catheterization are the gold standard techniques used for its detection. Cardiac magnetic resonance (CMR) can replace the invasive imaging modalities and provide a "one-stop shop" characterization of the cardiovascular system by measuring myocardial tissue structure, function and perfusion of the heart, as well as anatomy of and flow in the coronary arteries. In contrast to standard clinical magnetic resonance imaging (MRI) scanners, which are often operated at a field strength of 1.5 or 3 Tesla (T), a higher resolution and subsequent cardiac parameter quantification could potentially be achieved at ultra-high field, i.e., 7 T and above.

Unique insights into the pathophysiology of the heart are expected from ultra-high field MRI, which offers enhanced image quality in combination with novel contrast mechanisms, but suffers from spatio-temporal  $B_0$  magnetic field variations. Due to the resulting spatial misregistration and intra-voxel dephasing, these  $B_0$ -field inhomogeneities generate a variety of undesired image artifacts, e.g., artificial image deformation. The resulting macroscopic field gradients lead to signal loss, because the effective transverse relaxation time  $T_2^*$  is shortened. This affects the accuracy of  $T_2^*$  measurements, which are essential for myocardial tissue characterization. When steady state free precession-based pulse sequences are employed for image acquisition, certain off-resonance frequencies cause signal voids. These banding artifacts complicate the proper marking of the myocardium and, subsequently, systematic errors in cardiac function measurements are inevitable. Clinical MR scanners are equipped with basic shim systems to correct for occurring  $B_0$ -field inhomogeneities and resulting image artifacts, however, these are not sufficient for the advanced measurement techniques employed for ultra-high field MRI of the heart.

Therefore, this work focused on the development of advanced  $B_0$  shimming strategies for CMR imaging applications to correct the spatio-temporal  $B_0$  field variations present in the human heart at 7 T. A novel cardiac phase-specific shimming (CPSS) technique was set up, which featured a triggered  $B_0$  map acquisition, anatomy-matched selection of the shim-region-of-interest (SROI), and calibration-based  $B_0$  field modeling. The influence

of technical limitations on the overall spherical harmonics (SH) shim was analyzed. Moreover, benefits as well as pitfalls of dynamic shimming were debated in this study. An advanced  $B_0$  shimming strategy was set up and applied in vivo, which was the first implementation of a heart-specific shimming approach in human UHF MRI at the time.

The spatial  $B_0$ -field patterns which were measured in the heart throughout this study contained localized spots of strong inhomogeneities. They fluctuated over the cardiac cycle in both size and strength, and were ideally addressed using anatomy-matched SROIs. Creating a correcting magnetic field with one shim coil, however, generated eddy currents in the surrounding conducting structures and a resulting additional, unintended magnetic field. Taking these shim-to-shim interactions into account via calibration, it was demonstrated for the first time that the non-standard 3<sup>rd</sup>-order SH terms enhanced  $B_0$ -field homogeneity in the human heart. However, they were attended by challenges for the shim system hardware employed in the presented work, which was indicated by the currents required to generate the optimal 3<sup>rd</sup>-order SH terms exceeding the dynamic range of the corresponding shim coils. To facilitate dynamic shimming updated over the cardiac cycle for cine imaging, the benefit of adjusting the oscillating CPSS currents was found to be vital. The first in vivo application of the novel advanced  $B_0$  shimming strategy mostly matched the simulations.

The presented technical developments are a basic requirement to quantitative and functional CMR imaging of the human heart at 7 T. They pave the way for numerous clinical studies about cardiac diseases, and continuative research on dedicated cardiac  $B_0$  shimming, e.g., adapted passive shimming and multi-coil technologies.

## Zusammenfassung

Herz-Kreislauf-Erkrankungen zählen zu den häufigsten Todesursachen weltweit und werden bisher in der Regel mittels Echokardiographie, Nuklearkardiologie und Katheterisierung untersucht. Die kardiale Magnetresonanztomographie hat das Potential diese invasiven Bildgebungsmodalitäten zu ersetzen. Dabei können sowohl das kardiovaskuläre System anhand der myokardialen Gewebestruktur sowie der Funktion und Perfusion des Herzens als auch Anatomie und Blutfluss der Koronararterien während einer einzigen Untersuchung charakterisiert werden. Im Gegensatz zu den weit verbreiteten klinischen Magnetresonanztomographie- (MRT) Geräten, welche häufig bei magnetischen Feldstärken zwischen 1.5 und 3T operieren, ermöglichen Feldstärken von 7 Tesla und mehr eine höhere Auflösung und somit eine akkuratere Quantifizierung kardialer Parameter.

Die Ultrahochfeld-Magnetresonanztomographie (UHF-MRT) ermöglicht einzigartige Einblicke in die Pathophysiologie des Herzens. Neuartige Kontrastmechanismen und die verbesserte Bildqualität leiden jedoch unter Inhomogenitäten des statischen magnetischen  $B_0$ -Feldes. Aufgrund der daraus resultierenden falschen räumlichen Registrierung der Voxel und einer Dephasierung des Signals innerhalb eines Voxels erzeugen diese Inhomogenitäten des  $B_0$ -Feldes eine Vielzahl unerwünschter Bildartefakte, beispielsweise eine künstliche Deformation des Bildes. Die resultierenden makroskopischen Gradienten führen zu Signalverlust und beeinträchtigen die Messung der effektiven transversalen  $T_2^*$ -Relaxationszeit, welche für die Charakterisierung myokardialen Gewebes essentiell ist. Vor allem bei der Bildakquisition mittels der *Steady State Free Precession* Methode führen Inhomogenitäten des  $B_0$ -Feldes zu Signalauslöschungen. Die dadurch entstehenden Bildartefakte erschweren die genaue Markierung des Myokards und haben so systematische Fehler bei der Bestimmung der kardialen Funktion zur Folge. Klinische MRT-Geräte sind dabei mit sogenannten Shim-Systemen ausgestattet um die Inhomogenitäten des  $B_0$ -Feldes zu korrigieren. Für die kardiale UHF-MRT des Herzens sind diese standardisierten Shim-Systeme allerdings nicht mehr ausreichend.

Im Fokus stand deshalb die Entwicklung moderner Methoden zur räumlichen und zeitlichen Korrektur der  $B_0$ -Inhomogenitäten, welche als „Shimming“ bezeichnet wird, für die kardiale UHF-MRT. Es wurde eine neue, herzphasen-spezifische Shimming-Strategie untersucht, welche auf der getriggerten Datenaufnahme, der Optimierung für die Anatomie des Herzens, sowie der kalibrierungsbasierten Modellierung des korrigierenden Magnetfeldes basierte. Zudem wurde der Einfluss technischer Limitationen der Hardware auf das Shimming, insbesondere das dynamische Shimming, in dieser Studie erörtert. Schließlich wurde die entwickelte neuartige Shimming-Strategie in vivo evaluiert, welche zu diesem Zeitpunkt die erste Implementierung einer herzspezifischen Shimming-Strategie in der humanen kardialen UHF-MRT darstellte.

Räumlich wies das  $B_0$ -Feld, welches im Rahmen dieser Studie im Herzen gemessen wurde, lokalisierte Inhomogenitäten im Myokardium auf. Diese variierten zudem in ihrer Größe sowie der Stärke der  $B_0$ -Inhomogenität zeitlich über den Herzzyklus hinweg und ließen sich mittels anatomisch angepasstem, kalibrierungsbasiertem Shimming deutlich reduzieren. Erzeugt man ein korrigierendes Magnetfeld mittels einer Shim-Spule, so werden jedoch Wirbelströme in nahen leitenden Strukturen und weiterhin ein zusätzliches, unerwünschtes Magnetfeld erzeugt. Berücksichtigt man diese Wechselwirkungen zwischen den verschiedenen Shim-Spulen, konnte erstmalig der Vorteil von korrigierenden Magnetfeldern in der Form von Kugelflächenfunktionen der dritten Ordnung für die kardiale UHF-MRT gezeigt werden. Hierbei waren jedoch die erforderlichen, besonders starken Ströme in den Shim-Spulen zu berücksichtigen, welche über den Herzzyklus hinweg oszillierten und für dynamisches Shimming angepasst werden sollten. Die erste in vivo Anwendung der neu entwickelten Shim-Strategie stimmte gut mit den vorigen Simulationen überein.

Die vorgestellten technischen Entwicklungen stellen grundlegende Anforderungen an die quantitative und funktionelle kardialer UHF-MRT dar. Klinische Studien zu kardialen Erkrankungen wie der Herzinsuffizienz erscheinen nun ebenso in Reichweite wie weitere Forschung zu kardialem  $B_0$ -Shimming basierend auf angepasstem passiven Shimming sowie Multikanal-Spulen.



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## Frequent abbreviations

<u>Abbreviation</u>	<u>Description</u>
ACT	acoustic cardiac triggering
$B_0$	static magnetic field
$B_1$	electromagnetic radiofrequency field
CMR	cardiac magnetic resonance
CPSS	cardiac phase-specific shimming
DL	deep learning
ECG	electrocardiogram
FA	flip angle
FID	free induction decay
FOV	field-of-view
$\gamma$	gyromagnetic ratio
G	magnetic field gradient
GRAPPA	generalized partially parallel acquisition
IQR	interquartile range
LA	long axis
LV	left ventricle
mGRE	multi-gradient-echo
MRI	magnetic resonance imaging
$\phi$	signal phase
PD	proton density
pTx	parallel transmit
RF	radio-frequency
RV	right ventricle

Abbreviation	Description
RX	receive element
SA	short axis
SAR	specific absorption rate
SD	standard deviation
SH	spherical harmonics
SROI	shim-region-of-interest
SSFP	steady-state free precession
T	Tesla
TE	echo time
TR	repetition time
TX	transmit element
$T_1$	longitudinal relaxation time
$T_2$	transverse relaxation time
$T_2^*$	effective transverse relaxation time
UHF	ultra-high field
$\omega$	Larmor frequency
$\chi_m$	magnetic susceptibility

# 1 Introduction

A major cause of death worldwide is cardiovascular disease (1), which is typically diagnosed via echocardiography, nuclear cardiology, and catheterization as the gold standard techniques. These invasive imaging modalities could be replaced by cardiac magnetic resonance (CMR) imaging, which provides a "one-stop shop" solution for the characterization of the cardiovascular system - myocardial tissue structure, function and perfusion of the heart, as well as anatomy of and flow in the coronary arteries can all be measured in one imaging session (2,3). While 1.5 Tesla (T) or 3 T are standard field strengths for clinical magnetic resonance imaging (MRI) scanners, ultra-high field (UHF) MR systems are operated at 7 Tesla and above to potentially achieve a higher resolution and subsequent cardiac parameter quantification.

Unique insights into the pathophysiology of the heart are expected from UHF MRI, which offers enhanced image quality together with novel contrast mechanisms (4-6). These potential benefits of CMR imaging at 7 T are limited by inhomogeneities of the static magnetic ( $B_0$ ) field. The myocardium, surrounding lungs, and blood possess different magnetic susceptibilities and, along with the curved shape of the heart, cause intricate  $B_0$  field variations (7,8). These  $B_0$ -field inhomogeneities lead to spatial misregistration as well as intra-voxel dephasing and consequently to numerous unintended image artifacts, e.g., artificial image deformation (9). The induced macroscopic field gradients provoke signal loss due to truncated effective transverse relaxation times  $T_2^*$  (10). Extra temporal  $B_0$  field alterations among diverse cardiac phases and breathing positions are due to cardiac and respiratory motion (11).

Modern CMR imaging methods used at clinical field strengths of 1.5 T and 3 T to estimate cardiac function comprise the cine technique, at which images are acquired at multiple heart phases assess cardiac motion and function, based on balanced steady-state free precession (SSFP) techniques (12). In SSFP-based pulse sequences, a rapid concatenation of radiofrequency (RF) pulses and time periods free of RF excitation alternate (13). One example is the balanced SSFP method, for which the overall moment of magnetic field gradients applied for imaging has to be equalized (14). This method is seriously affected by  $B_0$ -inhomogeneities, which cause signal drop-offs and result in banding artifacts in the

acquired images (15). The latter impede the accurate marking of the myocardium in CMR imaging at 3 T (12), and, inevitably, lead to systematic errors in cardiac function measurements. Due to the increased  $B_0$ -inhomogeneities in comparison to 3 T, SSFP-based imaging techniques are not widely used for CMR at 7 T yet. Numerous rapid pulse sequences, e.g., spirals (16) and echo-planar imaging (17), also do not very well tolerate inhomogeneous  $B_0$ -fields. In addition, a narrow  $B_0$  field range is essential for designing optimized RF pulses, e.g., the parallel transmit (pTx) technique (18,19). These factors make  $B_0$  field corrections essential to avoid artifacts in CMR imaging (20).

Up to now,  $B_0$  inhomogeneities have been investigated for CMR applications at 1.5 T (21), 3 T (22), and 4 T (23). At UHF, the implementation of both an optimized saturation pulse train for human first-pass myocardial perfusion imaging (19) and the design of pTX RF pulses robust against respiration depend on a homogeneous  $B_0$ -field (11). Moreover, advanced shimming strategies tailored to CMR imaging methods, which have only been addressed for 1.5 T and 3 T (24), require additional technical improvements at 7 T. It is of interest whether the myocardial  $B_0$ -field inhomogeneities could be eliminated by shimming based on spherical harmonics (SH) functions or should be addressed by customized multi-coil hardware such as DYNAMITE (25,26).

In-depth knowledge of the higher, i.e., 3<sup>rd</sup>-order and above, SH constituents of the magnetic field and their spatio-temporal evolution also plays a critical role for dynamic shimming applications (27-30). Moreover, it is useful for the design of non-Cartesian k-space trajectories (31,32), for which detailed knowledge about the  $B_0$ -field enables high-precision correction of the MR scanner's gradient system imperfections via waveform pre-emphasis based on the gradient system transfer function. When this technique is applied without the use of a dynamic field camera (33), a shortened  $T_2^*$  signal decay resulting from  $B_0$ -field inhomogeneities is a major limitation at 7 T (34). Accurately determined input response functions for gradients and shims (35,36), which could be derived precisely by employing a dynamic field camera (37), allow for the determination of optimal k-space trajectories and facilitate adequate pre-emphasis (38-40).

A prominent example for the above-mentioned non-Cartesian k-space trajectories are spiral trajectories, which were proven to be beneficial for imaging of the brain at UHF (41). Here, important advantages are the measurement of more k-space data points during

a single readout and reduced acquisition times in contrast to standard linear sampling (42-45). However, the images are prone to blurring resulting from  $B_0$ -field inhomogeneities (46). Spiral k-space trajectories were recently applied for cardiac real-time MRI using pre-emphasis at 3 T (33) and 7 T (47), where uncorrected  $B_0$ -field fluctuations were shown to limit the application of this technique at 7 T.

Therefore, the scope of this work included the quantification of spatial  $B_0$ -field fluctuations in the human heart as well as their temporal variation over the cardiac cycle. In a next step, the key factors influential on the  $B_0$ -field homogeneity were evaluated, which included the triggered  $B_0$ -map acquisition, the anatomy-matched shim-region-of-interest (SROI) selection, and calibration-based  $B_0$ -field modeling in dedicated shim software. Following the optimization of these individual steps, an advanced shim strategy was set up and the workflow was investigated via magnetic field simulations. Here, static shimming was carried out to identify the importance of specific SH shim terms and the consequences of hardware limitations. Moreover, dynamic shimming was examined to discover the benefits of CPSS, i.e., shimming dynamically updated on cardiac phases. Initial results of the in vivo implementation of the developed advanced shim strategy were presented, and benefits as well as drawbacks of the latter were discussed.





## 2 Theory

*Major parts of the basic principles summarized hereafter consider common textbook knowledge, which is largely found in *The Handbook of MRI pulse sequences* (48), *Magnetic resonance imaging: physical principles and sequence design* (49), and *In vivo NMR spectroscopy: principles and techniques* (50). To preserve clearness, citations are only referred to where information goes beyond, in particular regarding the static magnetic  $B_0$  field and its correction, i.e., *shimming*.*

### 2.1 Spin polarization and relaxation

A nuclear spin located within a static magnetic  $B_0$  field shows a quantum-mechanical behavior, which can be described by a Hamiltonian according to the literature:

$$\hat{H}_z = -\gamma\hbar B_0 \hat{I}_z . \quad (1)$$

In this case, the  $B_0$  field directs to the  $z$ -direction of the coordinate system, and the  $z$ -component of the angular momentum operator  $\hat{I}$  is represented by  $\hat{I}_z$ .  $\hbar$  corresponds to the Planck's constant, and the gyromagnetic ratio is denoted by  $\gamma$ . Due to the angular momentum of a proton, known as the spin  $\vec{I}$ , a magnetic moment is induced:

$$\vec{\mu} = \gamma\hbar\vec{I} . \quad (2)$$

While a spin directing parallel to the  $B_0$  field is referred to as *spin up* or  $\uparrow$ , a spin aligned with the anti-parallel direction is referred to as *spin down* or  $\downarrow$ . The resulting potential energy levels  $E = -\mu \cdot B_0$  consequently split up, which is known as the Zeeman effect. For protons of spin  $\pm\frac{1}{2}$ , both states differ by  $\Delta E = E_{\downarrow} - E_{\uparrow} = \gamma\hbar B_0$ . Assuming an ensemble of non-interacting particles at the thermal equilibrium, the rate of corresponding

population probabilities  $P_{\uparrow,\downarrow}$  accounts for  $\frac{P_{\downarrow}}{P_{\uparrow}} = \exp\left(\frac{\gamma\hbar B_0}{k_B T}\right)$ .  $k_B$  denotes the Boltzmann constant, whereas  $T$  stands for the temperature. As a result,  $N$  spins feature the following macroscopic equilibrium magnetization or total magnetic moment  $\vec{M}_0$ :

$$\vec{M}_0 = N(P_{\downarrow} - P_{\uparrow})\vec{\mu} = \frac{N\gamma^2\hbar^2}{4k_B T} \vec{B}_0 . \quad (3)$$

The temporal evolution of the macroscopic magnetization  $\vec{M}$  results from Liouville's equation and is straightforward connected to the  $B_0$  field strength:

$$\frac{d}{dt} \vec{M} = -\gamma \vec{M} \times \vec{B}_0 . \quad (4)$$

Deflected spins tend to restore the initial magnetization  $\vec{M}_0$  via a relaxation process, which is described by the Bloch equations. The magnetization fraction  $M_z$  aligned with the  $B_0$  field direction is characterized by the longitudinal relaxation time  $T_1$ , while the fraction  $M_{x,y}$  perpendicular to the  $B_0$  field is linked to the transversal relaxation time  $T_2$ :

$$\frac{d}{dt} M_z = -\gamma (\vec{M} \times \vec{B}_0)_z + \frac{M_0 - M_z}{T_1} \quad (5)$$

$$\frac{d}{dt} M_{x,y} = -\gamma (\vec{M} \times \vec{B}_0)_{x,y} + \frac{M_{x,y}}{T_2} . \quad (6)$$

Hence, the temporal evolution of the three magnetization components is expressed as:

$$M_x = M_0 \exp\left(-\frac{t}{T_2}\right) \cos(\omega_0 t) \quad (7)$$

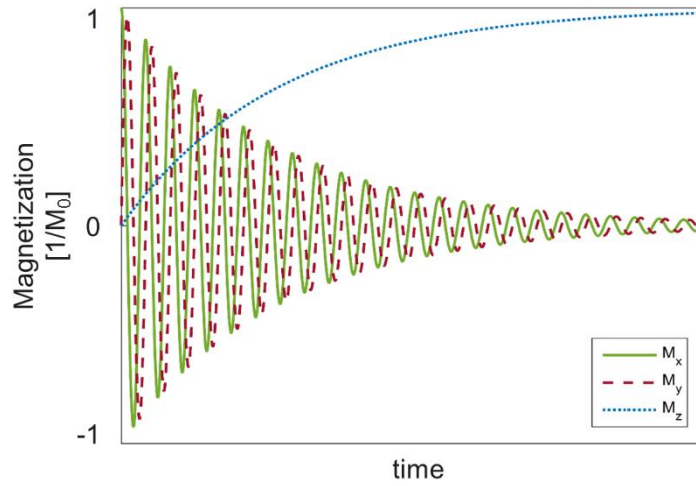
$$M_y = M_0 \exp\left(-\frac{t}{T_2}\right) \sin(\omega_0 t) \quad (8)$$

$$M_z = M_0 \left[1 - \exp\left(-\frac{t}{T_1}\right)\right] . \quad (9)$$

Beside relaxation processes, the transversal magnetization  $\vec{M}_{x,y}$  precesses around the  $B_0$  field direction with the so-called Larmor frequency  $\omega_0$  according to the Bloch equations:

$$\omega_0 = 2\pi\nu_0 = \gamma B_0 \quad . \quad (10)$$

The transversal magnetization  $\vec{M}_{x,y}$  induces a magnetic resonance (MR) signal, which has the shape of a free induction decay (FID), i.e., a damped sinusoidal function (Figure 1).



**Figure 1.** Relaxation processes for magnetization components due to the Bloch equations.

Local field variations  $\Delta B_0$  lead to decreased measurable transversal relaxation times  $T_2^*$ :

$$\frac{1}{T_2^*} = \frac{1}{T_2} + \gamma\Delta B_0 \quad . \quad (11)$$

The measurable radio-frequency (RF) induction signal, which is due to  $\omega_0$ , results from the spin density distribution  $\rho(\vec{r}, \nu)$  distinguished by locations  $\vec{r}$  and frequencies  $\nu$ :

$$s(t) = \iint \rho(\vec{r}, \nu) e^{-\frac{t}{T_2^*}} e^{2\pi i \nu t} d\vec{r} d\nu \quad . \quad (12)$$

The deflection of magnetization by a flip angle  $\alpha$  and the generation of an induction signal  $s(t)$  is achieved through an electromagnetic RF or  $B_1$  field of a certain duration  $\tau$ :

$$\alpha = \gamma \int_{t=0}^{\tau} B_1(t) dt \quad (13)$$

The complex  $B_1$  field can be decomposed into two constituents: the fraction rotating clockwise is termed the  $B_1^+$  field, and the fraction rotating counterclockwise the  $B_1^-$  field:

$$B_1^+ = \frac{B_{1,x} + iB_{1,y}}{2} \quad (14)$$

$$B_1^- = \frac{(B_{1,x} - iB_{1,y})^*}{2} \quad (15)$$

The  $B_1^+$  field is transmitted for signal excitation and interacts with the spins. Due to the reciprocity principle,  $B_1^-$  describes the field which induces the measurable MR signal  $s(t)$  (51). In practice, RF coils consist of multiple transmit elements instead of a single loop or antenna. Optimal image quality is achieved by a homogeneous combination  $B_{1,comb}^+(\vec{r})$ , which superimposes the  $B_{1,i}^+$  fields at position  $\vec{r}$  of the  $i = 1..n$  individual transmit elements with the complex signal amplitudes  $A$ :

$$B_{1,comb}^+(\vec{r}) = \sum_{i=1}^n A \cdot B_{1,i}^+(\vec{r}) \quad (16)$$

## 2.2 Image formation and pulse sequences

A constant Larmor frequency  $\omega_0$  across all observed spins does not provide insight into their spatial distribution. However, a spatial encoding of the measurable induction signal is realized by the application of magnetic field gradients, which could be generated across all three dimensions in a Cartesian coordinate system:

$$\vec{G}(\vec{r}) = \begin{pmatrix} G_x \\ G_y \\ G_z \end{pmatrix} = \begin{pmatrix} \partial B / \partial x \\ \partial B / \partial y \\ \partial B / \partial z \end{pmatrix} . \quad (17)$$

$G_x$ ,  $G_y$ , and  $G_z$  are commonly created by dedicated gradient coils and superimposed to the static  $B_0$  field. Thus, local  $B_0$  field gradients  $B_{0,loc}$  within the examined sample of spins are also encoded, which leads to a resulting Larmor frequency  $\omega(x, y, z)$  of:

$$\omega(x, y, z) = \gamma(B_0 + xG_x + yG_y + zG_z + B_{0,loc}) . \quad (18)$$

When magnetic field gradients are applied for a duration  $t$ , a spatially encoded induction signal is measurable – assuming an individual spin and negligible relaxation effects:

$$s(t) = s_0 e^{i\gamma \int_0^t \vec{G}(t') \vec{r} dt'} . \quad (19)$$

Subsequently, the k-space can be defined, which describes the local signal dependence generated by the magnetic field gradients  $\vec{G}(t)$ :

$$\vec{k} = \frac{\gamma}{2\pi} \int_0^t \vec{G}(t') dt' . \quad (20)$$

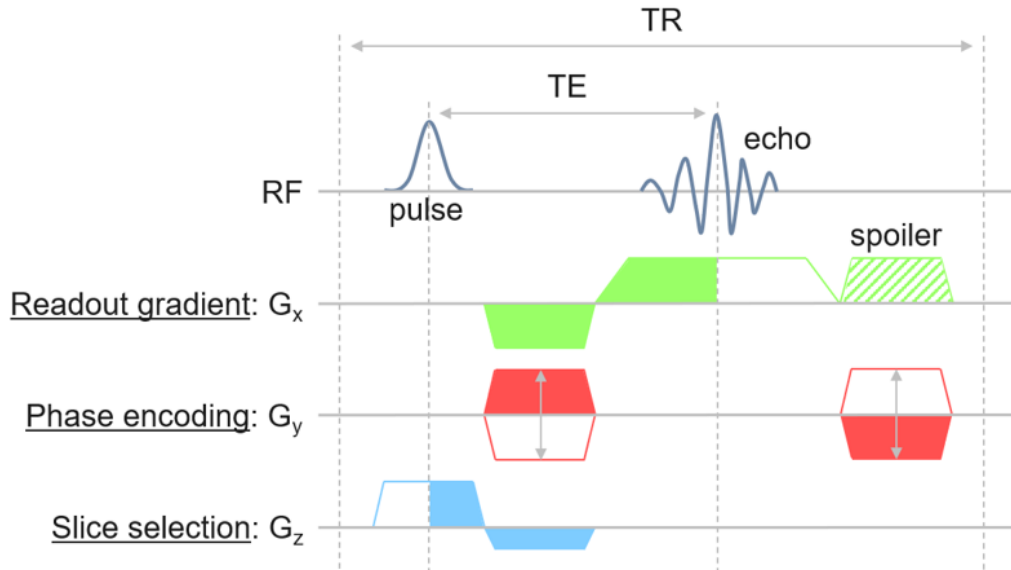
For an entire spin density distribution  $\rho(\vec{r})$  the measurable induction signal  $s(\vec{k})$ , which can successively be expressed through the k-space formalism, accounts for:

$$s(\vec{k}) = \int \rho(\vec{r}) e^{2\pi i \vec{k} \vec{r}} d\vec{r} . \quad (21)$$

Here, both k-space and the underlying image space are linked by the Fourier transform:

$$\rho(\vec{r}) = \int s(\vec{k}) e^{-2\pi i \vec{k} \vec{r}} d\vec{k} \quad . \quad (22)$$

In practice, the k-space cannot be sampled continuously. Hence, data is acquired on a grid described by the corresponding discrete Fourier pair. Both its magnitude and phase encode specific information, at which the latter reveals the  $B_0$  field. The number  $N$  of sampling steps and the field-of-view (FOV) define the spatial resolution by  $\Delta x = \frac{FOV}{N}$ . The entity of RF pulses and magnetic field gradients, which are applied to acquire data during an MR experiment, are referred to as pulse sequences. A common approach for sampling the k-space is the Cartesian trajectory, among which gradient echo-based (GRE) pulse sequences represent a major category and are explained successively (Figure 2).



**Figure 2.** Schematic illustration of a gradient-recalled echo (GRE) pulse sequence.

A slice-selective magnetic field gradient  $G_z$  is applied during the RF pulse to only excite spins within the desired imaging plane. Note that unwanted dephasing caused by  $G_z$  is canceled via an appropriate gradient  $G_z$  of inverse polarity. To address a certain line in  $y$ -direction of the k-space, signal phase-encoding along this dimension is achieved by a

dedicated gradient  $G_y$ . To sample data points on this k-space line, a third gradient  $G_x$ , which creates a frequency dependency of the spins and is termed readout gradient, is applied along the  $x$ -direction. The occurrent spin dephasing is recalled by an upstream  $G_x$  gradient of inverse polarity. As a result, a so-called gradient-echo is observed at which image data is acquired. The time span between RF pulse and echo formation is known as the echo time TE. Before the next RF pulse is applied after the repetition time TR, another  $G_y$  gradient rewinds the signal phase. Spoiling gradients are applied after each TR cycle to minimize the remaining transversal magnetization.

### 2.3 $B_0$ field mapping and phase unwrapping

The data acquisition assumes a homogeneous  $B_0$  field, while inhomogeneities cause local variations of  $\omega_0$ . In general, a net magnetic induction  $\vec{B}_{0,loc}$  occurs when an external magnetic field  $\vec{H}$  interacts with a sample of spins. The spin magnetization  $\vec{M}$ , which denotes the total magnetic moment  $\vec{m}$  per volume  $V$ , creates a magnetic induction of

$$\vec{B}_{0,loc} = \mu_0(\vec{H} + \vec{M}) . \quad (23)$$

Here,  $\mu_0$  stands for the vacuum permeability.  $\vec{M}$  depends on the magnetic susceptibility  $\chi_m$  of a material, which describes the grade of magnetization within a magnetic field  $\vec{H}$ :

$$\vec{M} = \chi_m \vec{H} . \quad (24)$$

$\chi_m < 0$  indicates diamagnetic materials, whereas substances with  $\chi_m > 0$  are termed paramagnetic.  $\chi_m \gg 1$  is characteristic for ferromagnetic materials. Due to Gauss's law,  $\vec{\nabla} \cdot \vec{B} = 0$ , there are no sources of the magnetic induction and  $\vec{B}$  has to be perpendicular to interfaces. Significant discontinuities of  $\chi_m$  consequently lead to strong  $B_0$  field inhomogeneities prominent at air-tissue boundaries, e.g., the heart-lung interface inside the human body.

To obtain quantitative information about present inhomogeneities, the  $B_0$  field has to be mapped across the shim-region-of-interest (SROI). This could be achieved using the Cartesian GRE pulse sequence, which allows data acquisition at multiple TE. Here, both an appropriate spacing of the TE to cover an adequately broad dynamic range of the MR signal, and a sufficiently large signal-to-noise ratio (SNR) at the longest TE are important. The SNR describes the ratio of the signal's mean and standard deviation.  $B_0$  field maps can subsequently be computed from the accumulated phase  $\Delta\varphi$  as its slope over TE:

$$\Delta B_0(x, y, z) = \frac{\Delta\varphi(x, y, z)}{\gamma\Delta TE} . \quad (25)$$

$B_0$  mapping techniques can be divided into two major approaches, one-dimensional (1D) projection-based and three-dimensional (3D) volumetric methods. 1D projection-based techniques sense the  $B_0$ -field along particular orientations and provide the benefit of short acquisition time (52,53). Projection  $B_0$ -mapping is advantageous to derive the spherical harmonics (SH) constituents of local  $B_0$ -fields, which are sufficiently tackled with 1<sup>st</sup>- and 2<sup>nd</sup>-order SH shim fields in most cases (54). Across the whole heart, which represents a large FOV and consequent complex  $B_0$  field distribution, 3D volumetric techniques are an appropriate tool. Here,  $B_0$  field maps are calculated voxel-wise for the complete SROI. This approach is employed in typical shim software such as the *BODETOX* application (26,55). In both cases, spatial and temporal phase wrapping has to be avoided and corrected where necessary.

A prerequisite for meaningful  $B_0$  mapping is the proper unwrapping of the signal phase. Uncorrected phase-wraps namely result in discontinuities in the reconstructed  $B_0$  maps, which are physically not plausible due to Maxwell's equations and limit their interpretability. Therefore, several methods exist to solve this issue. One option is the 3D *BEST PATH* algorithm (56). Quality maps, which are based on measures such as pseudo-correlation, phase derivative variance, or maximum gradient, are employed to unwrap highly reliable pixels first and less reliable pixels last. The 3D phase unwrapping paths are guided by the quality of the edges of the phase map. Another alternative is the phase region expanding labeler for unwrapping discrete estimates (*PRELUDE*) algorithm, which solves a cost function using a best-pair-first region merging approach (57). Phase



differences are penalized across boundaries. This algorithm is fast, automated, and applicable to arbitrary dimensions. For further improvement, the rapid open-source minimum spanning tree algorithm (*ROMEO*) has been introduced (58). Beside adapted measures for the quality maps and improved phase-unwrapping paths, single-step unwrapping can be performed across a fourth dimension, which enables temporal phase unwrapping across TE for  $B_0$  mapping.

## 2.4 Calibration-based shim field modeling

$B_0$  field variations could be removed, i.e., shimmed, by the application of correcting magnetic fields of identical shape but opposite polarity. The standard approach in most MR systems is the generation of shim fields in the form of SH functions up to 2<sup>nd</sup>- or 3<sup>rd</sup>-order (Table 1). Here, the underlying room-temperature shim coils, which create the individual SH-shaped magnetic fields, are located around the magnet bore (59,60). The SH functions solve the Laplace equation  $\Delta B_z = 0$  for the static magnetic field  $B_z$  aligned with the  $z$ -direction.  $B_z$  can subsequently be formulated as a linear combination of SH terms in spherical coordinates (61,62)

$$B_z(r, \varphi, \theta) = \sum_{n=0}^{\infty} \sum_{m=-n}^n C_n^m r^n P_n^m(\cos \theta) e^{im\varphi} \quad , \quad (26)$$

where the spherical position coordinates are expressed by  $r$ ,  $\theta$ , and  $\varphi$ .  $P_n^m$  represents the associated Legendre functions, which are of order  $n$  and degree  $m$ . Exemplary, all 1<sup>st</sup>- to 2<sup>nd</sup>-order SH terms as well as selected 3<sup>rd</sup>- (X3) and 4<sup>th</sup>-order (X4) terms are shown in along XY-, XZ, and YZ orientation in Figure 3.

Standard clinical scanners are equipped with 2<sup>nd</sup>-order SH shim coils, whereas state-of-the-art UHF MR systems offer correcting terms up to 3<sup>rd</sup>-order. 4<sup>th</sup>-order and above SH shim coils are up to now only integrated into research systems, e.g., by shim inserts (63). In any case, the shim coils influence each other via the generated magnetic fields.

**Table 1.** Spherical harmonics (SH) functions up to the 3<sup>rd</sup>-order. The SH terms are sorted by order and degree, and their abbreviation is assigned based on the dominating term in the Cartesian coordinates' formulation.

Order (n)	Degree (m)	Function	abbreviation
1	1	$x$	X
1	0	$z$	Z
1	-1	$y$	Y
2	2	$3(x^2 - y^2)$	X2-Y2
2	1	$3zx$	ZX
2	0	$z^2 - 1/2(x^2 + y^2)/2$	Z2
2	-1	$3zy$	ZY
2	-2	$6xy$	XY
3	3	$15x(x^2 - 3y^2)$	X3
3	2	$15z(x^2 - y^2)$	Z(X2-Y2)
3	1	$3/2 x[4z^2 - (x^2 + y^2)]$	Z2X
3	0	$z[z^2 - 3/2(x^2 + y^2)]$	Z3
3	-1	$3/2 y(4z^2 - (x^2 + y^2))$	Z2Y
3	-2	$30xyz$	XYZ
3	-3	$-15y(y^2 - 3x^2)$	Y3

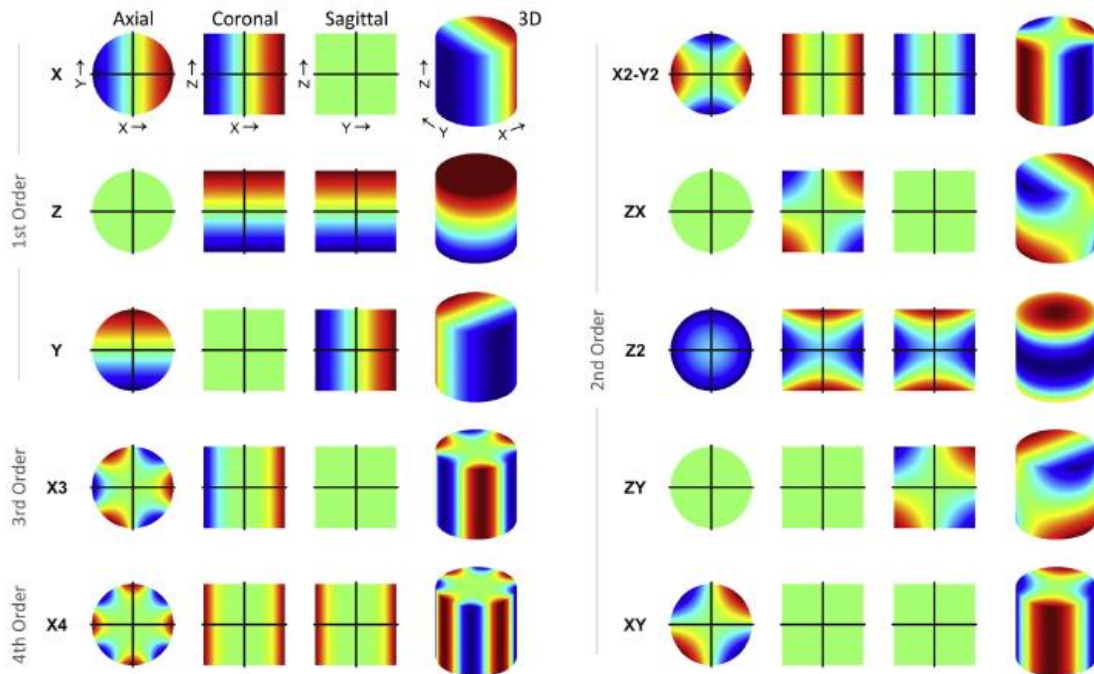
Shim-to-shim interactions provoke an individual treatment of each SH component and demand a shim system calibration to ensure a meaningful calculation of shim fields and appropriate currents (30). Moreover, the calibration procedure allows for an accurate determination of the total dynamic ranges, i.e., the maximum shim strength of each coil. The final calibration matrix  $A$  contains all information on the SH self- and cross-terms:

$$s = -I \cdot A^{-1} \quad . \quad (27)$$

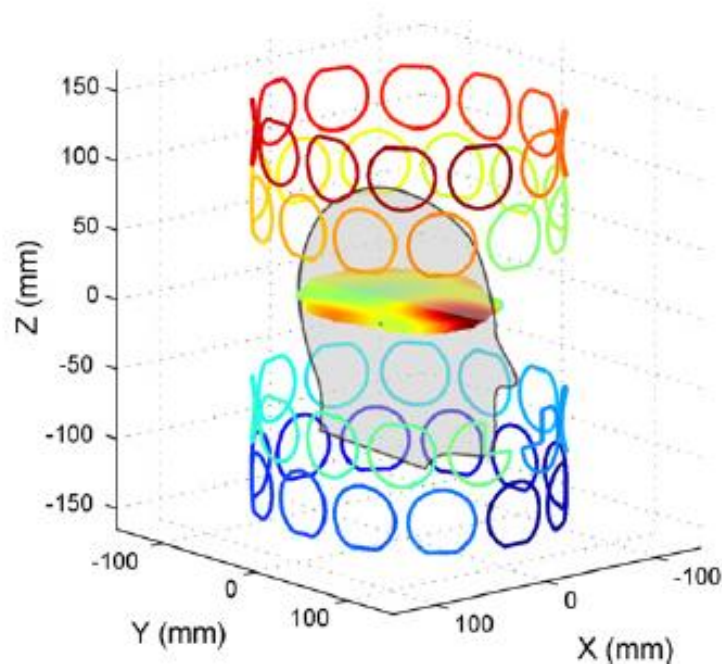
$A$  allows to derive the optimal shim settings  $s$  from the  $B_0$ -field before shimming with its SH components  $I$  and enables non-iterative single-step adjustments (62).

Beyond classical  $B_0$  shimming based on SH functions, a number of advanced concepts for magnetic field modeling have recently been developed. A widely used approach is the dynamic multi-coil technique (DYNAMITE), where numerous shim coil loops are placed around the subject to generate  $B_0$  field basis sets of much higher complexity than low-order SH functions (Figure 4) (25,26). Similar to SH-based shimming, the amplitudes  $C_n^m$  of the underlying non-orthogonal basis set of  $B_0$  fields are determined for optimal homogeneity.

Moreover, the AC/DC approach drives individual elements of an RF receive coil array by DC currents (64). In this way,  $B_0$  field homogeneity superior to 3<sup>rd</sup>-order SH shimming could be achieved. The integrated parallel reception, excitation, and shimming (iPRES) technique also combines both RF and  $B_0$  shimming technology (65). Since arranging the shim coils in the same localized setup is complicated for CMR measurements due to different body shapes and sizes, only SH-based  $B_0$  shimming is considered in this work. Multi-coil hardware for CMR imaging may be investigated in future studies.



**Figure 3.** Schematic illustration of SH functions. Shown are all 1<sup>st</sup>- and 2<sup>nd</sup>-order together with selected 3<sup>rd</sup>- and 4<sup>th</sup>-order terms on a cylindrical volume, which represents the typical case inside the bore of an MR system. Adapted with permission from Reference (66).



**Figure 4.** Dynamic multi-coil technique for  $B_0$  shimming of the human brain. In the setup shown above 48 individual shim coil loops are arranged in four rows to correct the measured  $B_0$  field distribution. Adapted with permission from Reference (26).

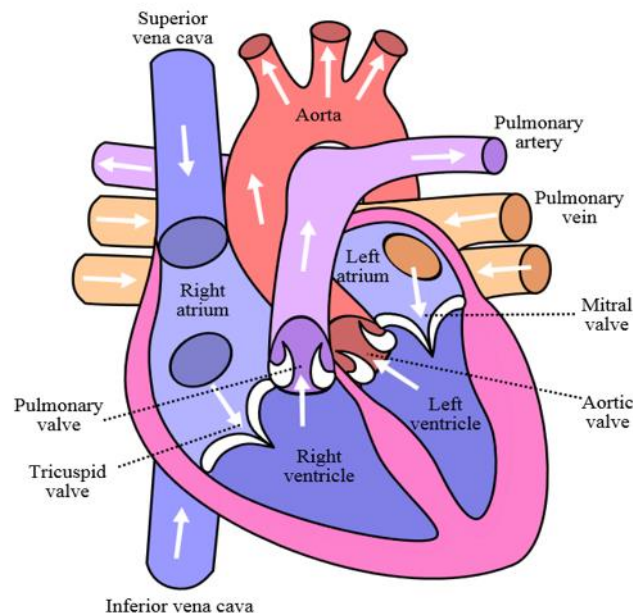
## 2.5 Anatomy and function of the human heart

When CMR image and  $B_0$  field data are acquired, several specialties have to be taken into account due to the shape of the heart as well as its function. Major aspects include double-oblique slice orientations to accurately determine volumetric parameters and the need for triggering because of cardiac motion, both of which are elucidated hereafter.

In general, the heart is the muscular pump for blood circulation in the systemic and the pulmonary system. The left-sided chambers split into the left atrium and the left ventricle with the aorta as its outlet. The left-sided muscle, e.g., the myocardium, is the driving force for the systemic circulation, distributing highly oxygenated blood through the body. The right-sided chambers split into the right atrium and the right ventricle, which are part of the pulmonary system and use the truncus pulmonalis as outlet (Figure 5).

To characterize the anatomy of the heart and cardiac function with CMR, the common image orientations are on the one hand the long-axis (LA) view, in which both the left and right ventricles and atria are visible similar to Figure 5. And on the other hand, the so-called short-axis (SA) view covers ventricular imaging slices perpendicular to the septum to properly monitor the contraction and expansion of the myocardium.

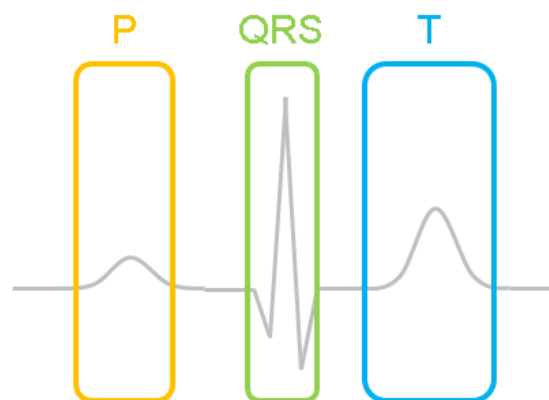
The right-ventricular myocardium fulfills the function of circulating the oxygen-deficient blood throughout the lungs to the left heart. Left and right ventricle are separated by the interventricular septum, while the left and right atria are separated by the interatrial septum. The atria and ventricles are divided by the mitral valve on the left side, and the tricuspid valve on the right side. In conjunction with the myocardial contraction, the aortic and pulmonary valves are opened, while the mitral and tricuspid valve are closed, which regulate and direct the circulation of the blood. The cardiac contractions follow a rhythmic sequence of contraction (systole) and relaxation (diastole) of the myocardium, allowing for ventricular filling before the next contraction. This temporal evolution forms the electrocardiogram (ECG).



**Figure 5.** Schematic illustration of the human heart. Adapted from Reference (67).

The electric activation is initiated at the sinus node, which is the impulse generator of the heartbeat and determines the heart rate. The activation moves on through the atria, which contract at the same time and pump the blood into the heart chambers. In the ECG, this correlates to the P wave (Figure 6). Afterwards the electrical excitation reaches the atrioventricular node, acting as a gatekeeper between atria and ventricles for the electrical activation, which then is distributed throughout the ventricular electrical conduction system. As a consequence, both chambers contract, which is indicated by a large spike termed the QRS complex of the ECG. In a final step, both ventricles relax again, which is represented by the T wave. The most distinct feature of the ECG is the pronounced R wave, which is consequently selected as the trigger signal. Due to the slow cardiac motion in diastole, image data is often acquired during this cardiac phase to reduce motion artifacts.

The interaction with electromagnetic fields generated by the gradient system and the liability to the magnetohydrodynamic effect form limitations of the ECG. In contrast, another technique called acoustic cardiac triggering (ACT) addresses the phonocardiogram. The first heart tone, which results from the systolic closure of the atrioventricular valves, is traced here. The trigger signal quality relies on accurate positioning of the stethoscope and could be disturbed by potential patient breathing and tentative background noise. These findings were demonstrated in an earlier study, where ACT was checked against vector ECG and pulse oximetry triggering (68).



**Figure 6.** Schematic illustration of the electrocardiogram (ECG) of the human heart.

## 3 Methods

### 3.1 Experimental setup

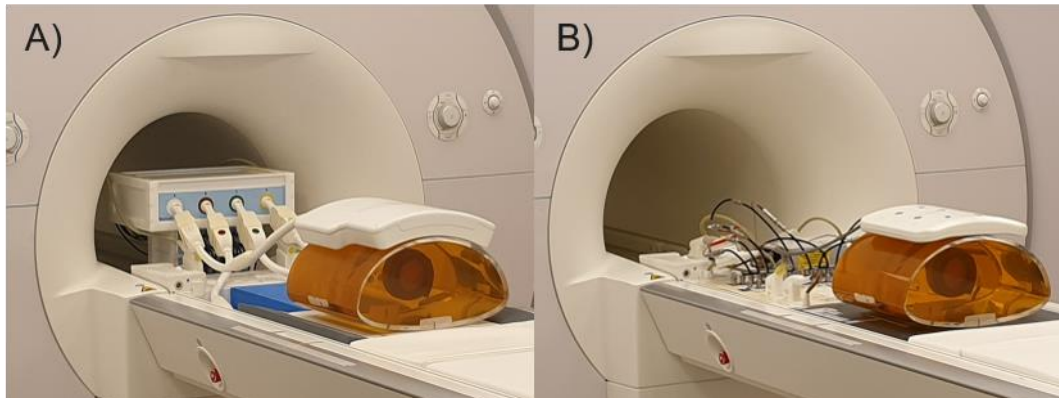
All data acquisition was carried out on a 7T whole-body MR scanner (MAGNETOM™ *Terra*, Siemens Healthineers, Erlangen, Germany), which is visualized in Figure 7. The magnet itself, which had a bore diameter of 60 cm, was cooled by the “Zero Helium boil-off” technology. In this way, minimum evaporation of helium was enabled (69). The 7T MR scanner was equipped with a gradient system capable of creating a maximum strength of 80 mT/m and a slew rate of 200 T/m/s. In comparison to 3T MR scanners, the SNR was doubled, and an in-plane resolution of 0.2 mm could be achieved for neurological applications (70). Up to 64 channels are available for RF signal receive coils. It has to be noted that this 7T *Terra* MR scanner has only been cleared for neurological and musculoskeletal clinical surveys by the US Food and Drug Administration (FDA) up to now (71). Examinations of the heart were only allowed for dedicated research purposes.



**Figure 7.** 7T *Terra* whole-body MR scanner for conducting *in vivo* experiments in human volunteers, patients, and large animals. The MR scanner, which was installed at the Comprehensive Heart Failure Center (CHFC) as part of the University Hospital Würzburg, facilitated state-of-the-art technologies such as parallel signal transmission.

At the beginning, the *in vivo* image acquisition on the 7T *Terra* MR scanner was performed with a commercial single-channel transmit (1Tx) / sixteen-channel receive (16Rx) RF coil (MRI Tools, Berlin, Germany). The modular RF coil design, which was tailored to the human thorax, consisted of an anterior and posterior part (Figure 8A). The limitation to 1Tx signal transmission was a significant drawback, which prevented the implementation of  $B_1^+$  shimming to improve the transmit field homogeneity. At 7 T, initial results demonstrated that  $B_1^+$  shimming improved the SNR along with line profiles across the heart (4).

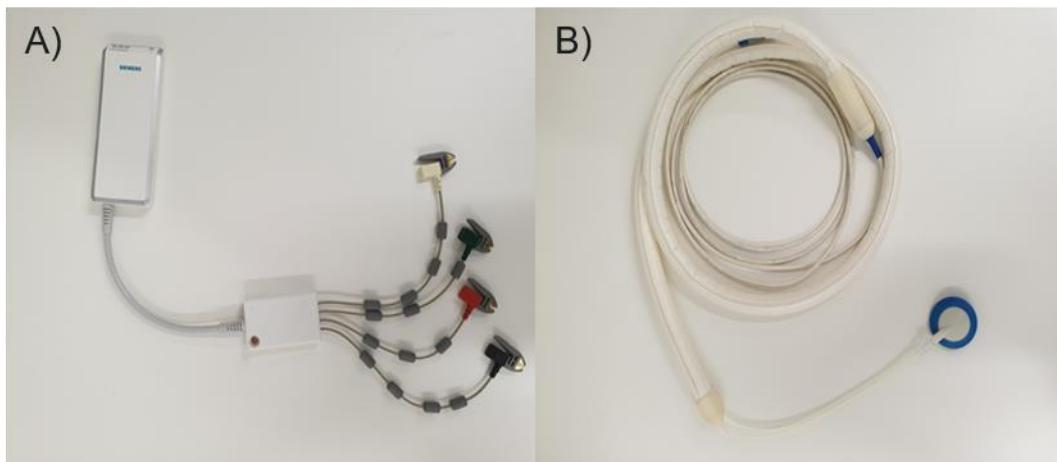
To homogenize the  $B_1^+$  field in an optimal way, a new RF coil capable of parallel transmission (pTx) was developed (Figure 8B), which employed eight elements for signal transmission (8Tx) and sixteen for reception (16 Rx).  $B_1^+$  shimming via adjustment of the signal phases for all transmit elements is challenging due to energy deposition constraints. Therefore, electromagnetic simulations were conducted for the human body models *Duke* and *Ella* (IT'IS Foundation, Zurich, Switzerland) in *CST Microwave Studio* (Computer Simulation Technology AG, Darmstadt, Germany) to account for safety aspects. The final product version enabled image quality superior to the commercial RF coil (72,73).



**Figure 8.** Radio-frequency coils for *in vivo* CMR of the human heart. The commercial RF coil operated only in single-channel transmit (1Tx) mode (A). In contrast, the new RF coil enabled parallel transmission (pTx) and allows for an optimization of the  $B_1^+$  field homogeneity (B).  $B_1^+$  shimming was realized by manipulation of the signal amplitude and phase for each transmit element.



Throughout all *in vivo* human examinations, two cardiac monitoring techniques were applied to continuously keep track of cardiac activity (74). The functionality of both techniques and related hardware devices, namely the scanner-integrated electrocardiogram (ECG) and an acoustic cardiac triggering (ACT) system (EasyACT, MRI Tools), has already been described in Section 2.5 (Figure 9).



**Figure 9.** Hardware devices for applied cardiac triggering techniques. The ECG device addressed the electrocardiogram (A), whereas ACT employed the phonocardiogram (B).

## 3.2 Spatio-temporal $B_0$ variations

### 3.2.1 $B_0$ -field measurements

This study was approved by the Ethics Committee of the University of Würzburg (7/17-sc). Ten healthy humans volunteered to be scanned for this project and gave their written informed consent. A training group was set up of four subjects to assemble an imaging protocol for the quantification of spatio-temporal  $B_0$  field variations. The imaging protocol was carried out for the study group of additional six subjects (3 female, 3 male), who were  $23.7 \pm 2.7$  years old, had a weight of  $73.5 \pm 15.4$  kg, and a height of  $176.5 \pm 9.4$  cm.

Spatial  $B_0$  field distributions across the heart were acquired at a trigger delay of  $490 \pm 66$  ms during mid-diastole with the following sequence settings: TE1/TE2/TE3/TE4/TE5 = 1.7/2.8/4.0/6.0/9.7 ms, TR = 401 ms, matrix =  $128 \times 128$ , FOV =  $300 \times 300$  mm<sup>2</sup>, number of slices = 3, slice thickness = 6.0 mm, slice separation = 1.2 mm, flip angle = 25°, GRAPPA = 3, and number of segments = 29. A typical breath-hold duration of 15 seconds allowed for the measurement of three transversal mid-ventricular slices.

To measure the temporal  $B_0$  field fluctuations over various cardiac phases, several sequence parameters such as TR and number of TEs had to be modified. The eight cardiac phases, at which the field map data were acquired, were equally distributed over an RR interval of  $970 \pm 127$  ms. The following parameters were set: TE1/TE2/TE3 = 1.7/2.8/4.0 ms, TR = 90 ms, matrix =  $128 \times 128$ , FOV =  $320 \times 320$  mm<sup>2</sup>, number of slices = 3, slice thickness = 6.0 mm, slice separation = 1.2 mm, flip angle = 40°, GRAPPA = 3, and number of segments = 15. Note that the data for each slice was measured in an individual breath-hold of 15 seconds net time.

### 3.2.2 Evaluation of $B_0$ maps

At first, the  $B_0$  maps were reconstructed from the measured field map data by voxel-wise linear regression of the signal phase evolution over echo time according to Section 2.3. Spatial phase-unwrapping was performed using the PRELUDE algorithm of the FMRIB Software Library (FSL) from the Oxford Center for Functional MRI of the Brain (57,75), which was relatively robust and considered the gold standard (76). It has to be noted that the  $B_0$  maps were calculated in *BODETOX* and then exported from the shim software.

Afterwards, the standard deviations (SD) and interquartile ranges (IQR) of the spatial magnetic field distributions were computed for the manually segmented regions-of-interest in *MATLAB* R2015b (MathWorks Inc, Natick, MA, USA). For both the left- and right-ventricular myocardium, the temporal  $B_0$  field fluctuations were obtained as the differences  $\Delta$ SD and  $\Delta$ IQR between systolic and diastolic field map data. In detail, the 25<sup>th</sup> and 75<sup>th</sup> percentiles of the  $B_0$  distribution allowed for a quantification of the IQR.

### 3.3 Heart-specific $B_0$ shim strategy

#### 3.3.1 Shim-region-of-interest selection

The 7T MR scanner used in this work featured a partial 3<sup>rd</sup>-order SH shim system, allowing for  $B_0$ -shimming beyond 1<sup>st</sup>- to 2<sup>nd</sup>-order SH terms. The built-in hardware enabled the generation of the 3<sup>rd</sup>-order SH terms  $Z_3$ ,  $Z_2X$ ,  $Z_2Y$ , and  $Z(X_2-Y_2)$ . Shim coils for magnetic field modeling based on the  $X_3$ ,  $Y_3$ , and  $XYZ$  functions were not integrated. To generate a uniform  $B_0$  field inside the heart using the shim system at hand, a precise SROI selection was proven to be beneficial (12,77). Thus, three approaches based on a transversal SROI cuboid using the vendor-supplied shimming platform were compared: (i) volume-selective shimming covering the whole heart, (ii) slab-selective shimming of the three acquired slices, and (iii) slice-selective shimming of merely the central slice. Beyond this, no other anatomy-matched SROI adjustment was feasible. The vendor-supplied  $B_0$  mapping was executed without cardiac triggering and in exhaled breath-hold position, while making use of the shortest available first TE and inter-echo spacing. The pulse sequence featured the following default parameters (78): TE1/TE2 = 1.02/3.06 ms, TR = 4.3 ms, matrix =  $64 \times 64$ , FOV =  $282 \times 282$  mm<sup>2</sup>, number of slices = 52, slice thickness = 4.4 mm, slice separation = 0.9 mm, flip angle = 4°, GRAPPA = 2, and number of segments = 1.

#### 3.3.2 Calibration of spherical harmonics shim system

A careful system calibration is a requirement to determine the total dynamic range of each SH shim term and essential cross-term corrections. For this purpose, an experiment using a spherical oil phantom and a 1TX / 2RX birdcage coil (Siemens Healthineers) was set up (79). Each shim term was modified in seven steps, which utilized 10% of the dynamic range for the linear gradients, and 30% to 50% for the higher orders, relative to a reference  $B_0$  map. The parameter settings for the pulse sequence were: TE1/TE2/TE3/TE4 = 1.0/1.3/2.0/4.0 ms, TR = 30 ms, matrix =  $108 \times 128$ , FOV =  $186 \times 220$  mm<sup>2</sup>, number of slices = 64, slice thickness = 2.7 mm, and flip angle = 25°.

After reconstructing the  $B_0$  field maps, the underlying SH components were derived from the computed magnetic field distributions. The calculation of the adequate shim fields, i.e., each SH constituent in inverse polarity, was performed by constrained least-squares fitting (9,80). Compared to other constrained nonlinear optimization methods, the applied Levenberg-Marquardt algorithm was found to be most resilient against changes in starting point values (81). The limited dynamic ranges of the shim coils could then be accounted for in the optimization process. In other words, the shim field was regularized to the hardware capabilities. Based on the determined SH components in the reconstructed  $B_0$  map, a shim field and corresponding shim currents were computed. All magnetic field modeling steps could be performed in the *BODETOX* software environment.

### 3.3.3 Simulation of static shimming

The spatial pattern of  $B_0$  field variations was addressed on  $B_0$  maps at a mid-diastolic cardiac phase, which minimized the influence of cardiac motion due to ventricle contraction during systole (18). Regarding the correction of the SH components present in the measured  $B_0$  fields, it was investigated whether the dynamic range of each shim coil was adequate to balance the respective SH term. This task was achieved by not restricting the currents for the least-squares optimization during  $B_0$  field shaping. Beyond, three kinds of shims were simulated to analyze the impact of the 3<sup>rd</sup>-order terms: 2<sup>nd</sup>-order only, 2<sup>nd</sup>- plus 3<sup>rd</sup>-order incorporating hardware restrictions, and 2<sup>nd</sup>- plus 3<sup>rd</sup>-order neglecting those restrictions. In each case, the un-shimmed  $B_0$  field served as the input to simulate the specific shim. The term un-shimmed refers to the system's default shim settings, which employed less than 5% of the maximum current in all shim coils.

### 3.3.4 Simulation of dynamic shimming

For eight equally-spaced phases of the cardiac cycle the  $B_0$  field in the heart was monitored to resolve temporal shim field variations. The dynamic alterations of required shim currents were determined by the anatomy-matched SROI selection and calculation

of correcting magnetic fields for each cardiac phase. Since the MR system at hand was not provided with the hardware essential for cardiac phase-specific shimming (CPSS), it was investigated whether an averaged static shim, which facilitated the mean of all eight CPSS fields, would be beneficial for applications such as cine imaging.

### 3.3.5 Advanced *in vivo* $B_0$ shimming

The previous findings paved the way for an advanced shim strategy, which was then made available for *in vivo* shimming and comprises of the following procedure (82,83):

1.  $B_0$  maps were measured for three slices at a mid-diastolic cardiac phase in a triggered fashion with ACT;
2. The anatomy-matched SROI adjustment was carried out by hand on the magnitude images for all slices together with a voxel-specific field-gradient boundary value to eliminate outliers;
3. SH-based magnetic field optimization was performed in the *BODETOX* software environment and the derived shim fields in  $\text{Hz}/\text{cm}^n$ , where  $n$  denotes the order of the SH components, were converted to shim coil currents units;
4. The calculated shim coil currents were employed on the MR system, and step 1 was iterated to validate the derived  $B_0$  field.

The acquired field map data were copied from the MR system to a dedicated computer for data analysis and imported into the *BODETOX* software environment. The reconstruction of field map data was executed as delineated in Section 2.3, and the anatomy-matched SROI was subsequently traced by the user on the magnitude images. In the next step, the optimal shim fields and underlying currents were calculated as specified in Section 2.4. The obtained hardware settings, which generated the correcting  $B_0$  field, were saved as a text file and applied to the MR system via a batch script. The entire procedure required approximately 6-8 minutes, in which most of the time was needed for the adjustment of the anatomy-matched SROI by the user and the generation of the derived shim fields via setting of the currents on the scanner console.

The initial  $B_0$ -field maps, which were acquired as the basis for the shim field computations, were then checked against those measured after the application of these shim fields with regard to homogeneity. For this purpose, the SDs of the  $B_0$ -field within the heart were calculated as a comparative measure.

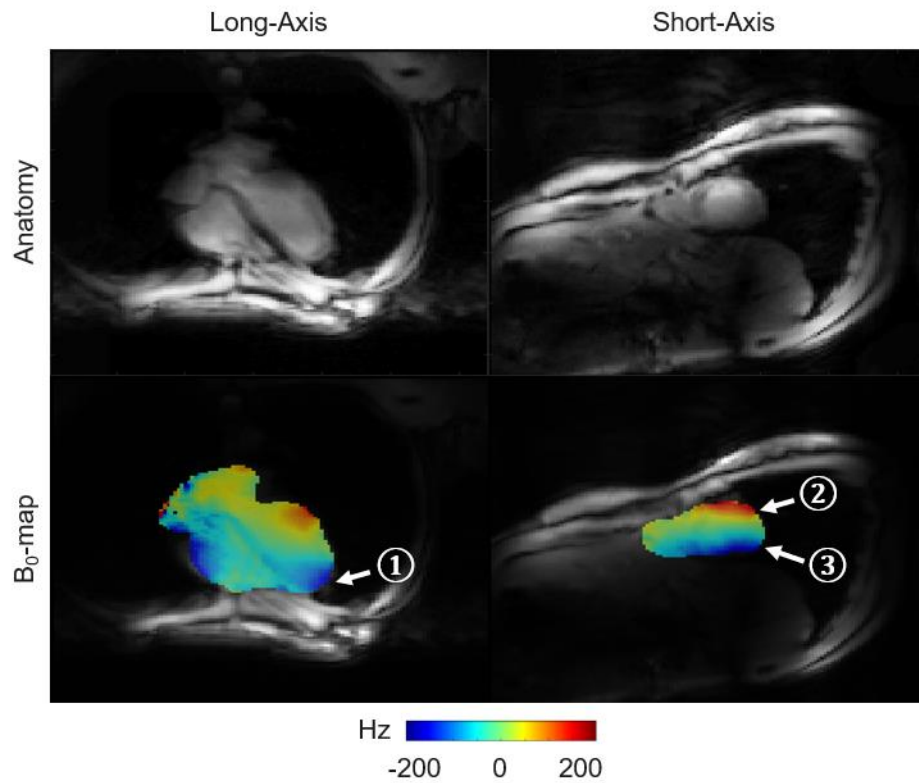
## 4 Results

*The investigations on  $B_0$  shimming of the human heart, including the analysis of spatio-temporal  $B_0$  field variations as well as static and dynamic cardiac phase-specific shimming, are published to some extent in (84).*

### 4.1 Spatio-temporal $B_0$ variations

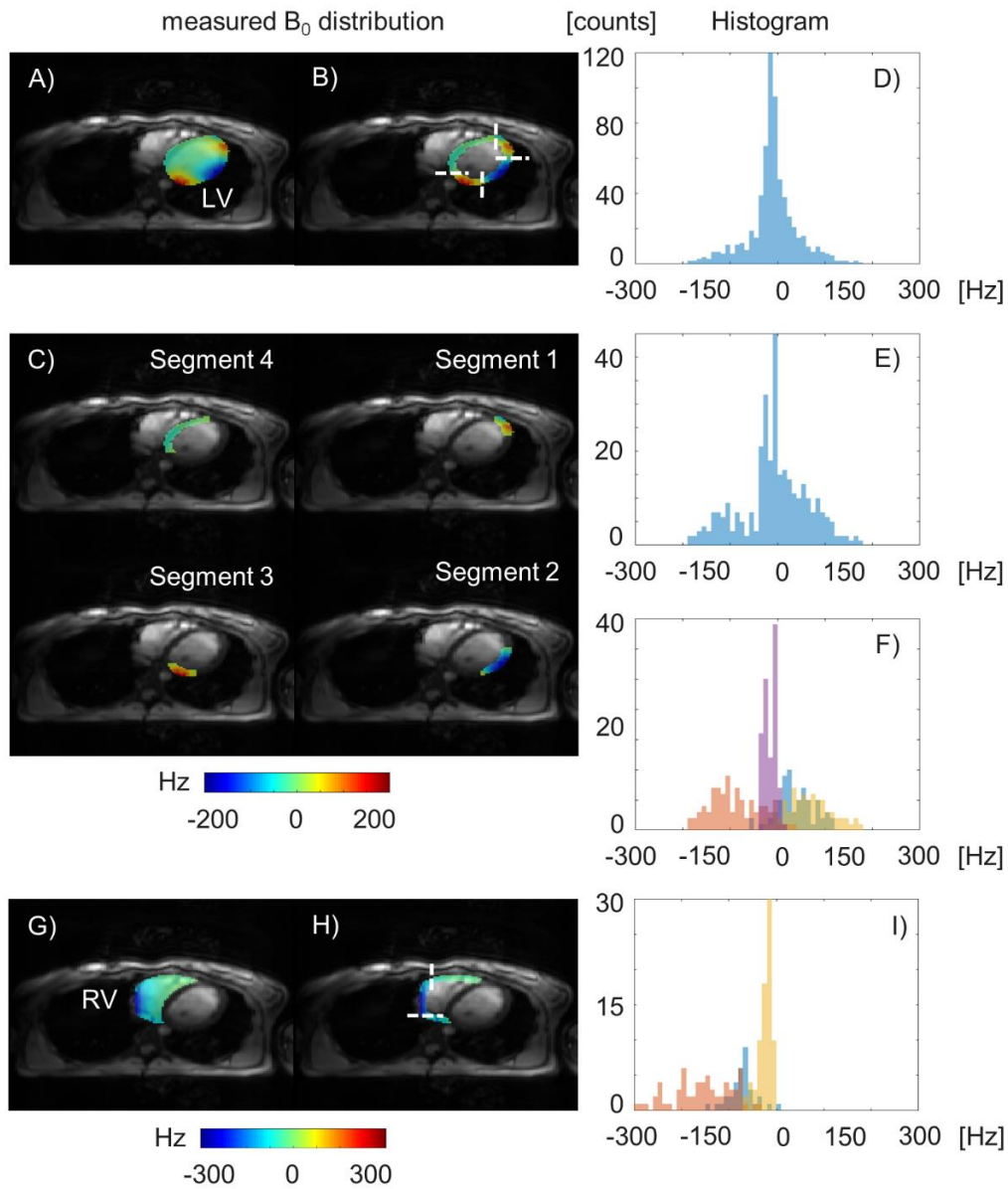
Figure 10 displays the spatial  $B_0$ -field distribution in both LA and SA views. Severe negative  $B_0$ -field variations were present near the apex in the LA view. Beyond that, strong  $B_0$ -field variations were found at the anterior and posterior wall of the left-ventricular myocardium in the SA view. A segment-wise histogram analysis revealed that the -100 Hz to 100 Hz interval covers most data points. However, localized spots of exceptional values were found in the left- and right-ventricular myocardium (Figure 11).

Temporal variations of the  $B_0$  field in the myocardium were observed over the cardiac cycle (Figure 12). In addition, a slice-to-slice variation of the  $\Delta SD$  in the left-ventricular myocardium arose. A mean  $\Delta SD$  of  $10 \pm 5$  Hz and  $\Delta IQR$  of  $19 \pm 12$  Hz between systole and diastole, for which cardiac phases similar to subject 3 were monitored, were found for all slices and subjects. The right-ventricular  $\Delta SD$  added up to  $17 \pm 9$  Hz and  $\Delta IQR$  to  $17 \pm 10$  Hz averaged over all slices and subjects. Considering the septum, which is exemplary highlighted in Figure 11C (segment 4), a temporal  $B_0$ -field fluctuation of  $\Delta SD_{Sep} = 3 \pm 2$  Hz was measured. As a result, the smallest  $\Delta SD$  and  $\Delta IQR$  occurred in the septum in comparison to both ventricles. Center frequency changes yielded  $\Delta F_{0,LV} = 8 \pm 6$  Hz and  $\Delta F_{0,RV} = 16 \pm 11$  Hz averaged over all subjects and slices.

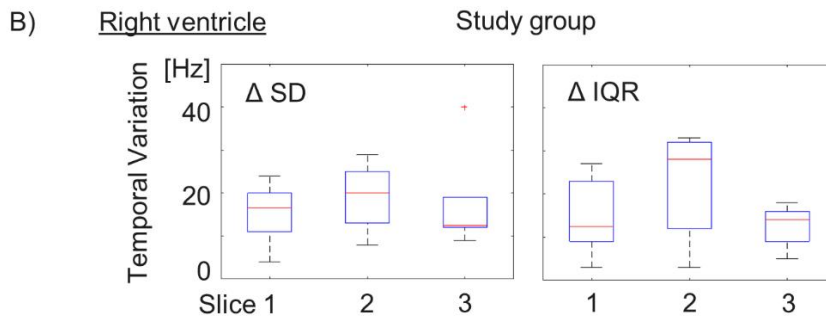
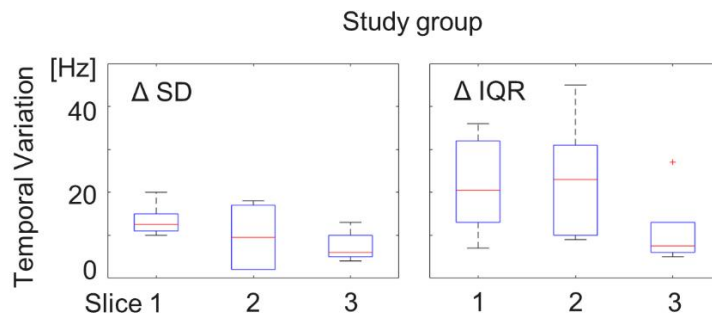
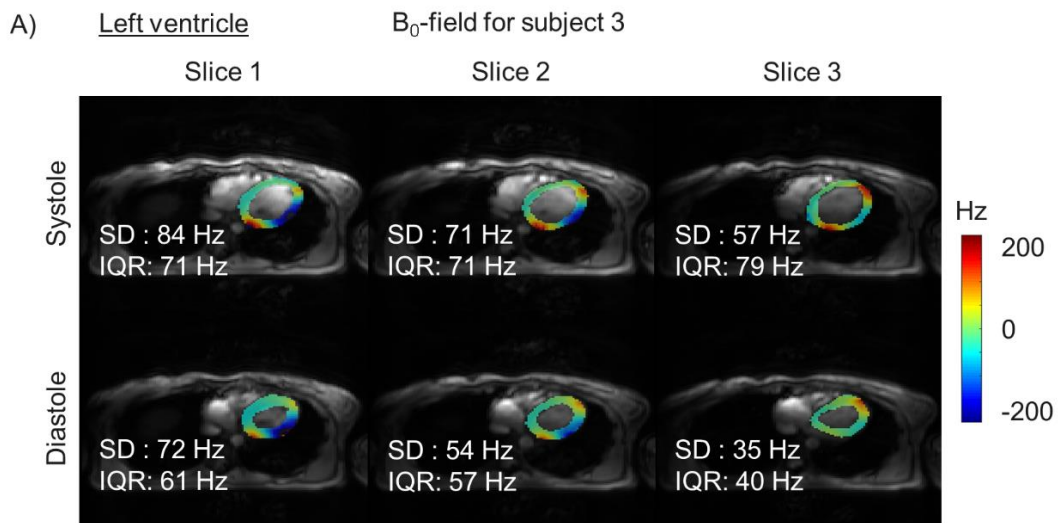


**Figure 10.**  $B_0$  field distribution inside the human heart in standard anatomical views. Distinct negative  $B_0$ -field inhomogeneities are present near the apex in the long-axis (LA) view (1). Precise  $B_0$ -field variations were also found at the anterior (2) and posterior (3) wall of the left-ventricular myocardium in the short-axis (SA) view. The contrast of the anatomical images was modified for visualization, employing the “*adaphisteq*” *MATLAB* function, which executes contrast-limited adaptive histogram equalization. Adapted from Reference (84).





**Figure 11.** Spatial  $B_0$ -field distribution across the heart. Displayed are the calculated  $B_0$  distributions (left) and underlying histograms (right) for the whole left ventricle (A), the left-ventricular myocardium (B), and four segments of the latter (C). The histograms D-F correlate with the measured  $B_0$  distributions A-C at a time. In F, the color blue represents segment 1, red segment 2, yellow segment 3, and purple segment 4. The  $B_0$  distribution across the entire right ventricle is visualized in G. Once more, the  $B_0$  field variations in the myocardium (H) are highly relevant and visualized in histogram I. In I, the color yellow correlates with the anterior segment in H, blue with the inferior segment, and red with the lateral segment. Adapted from Reference (84).

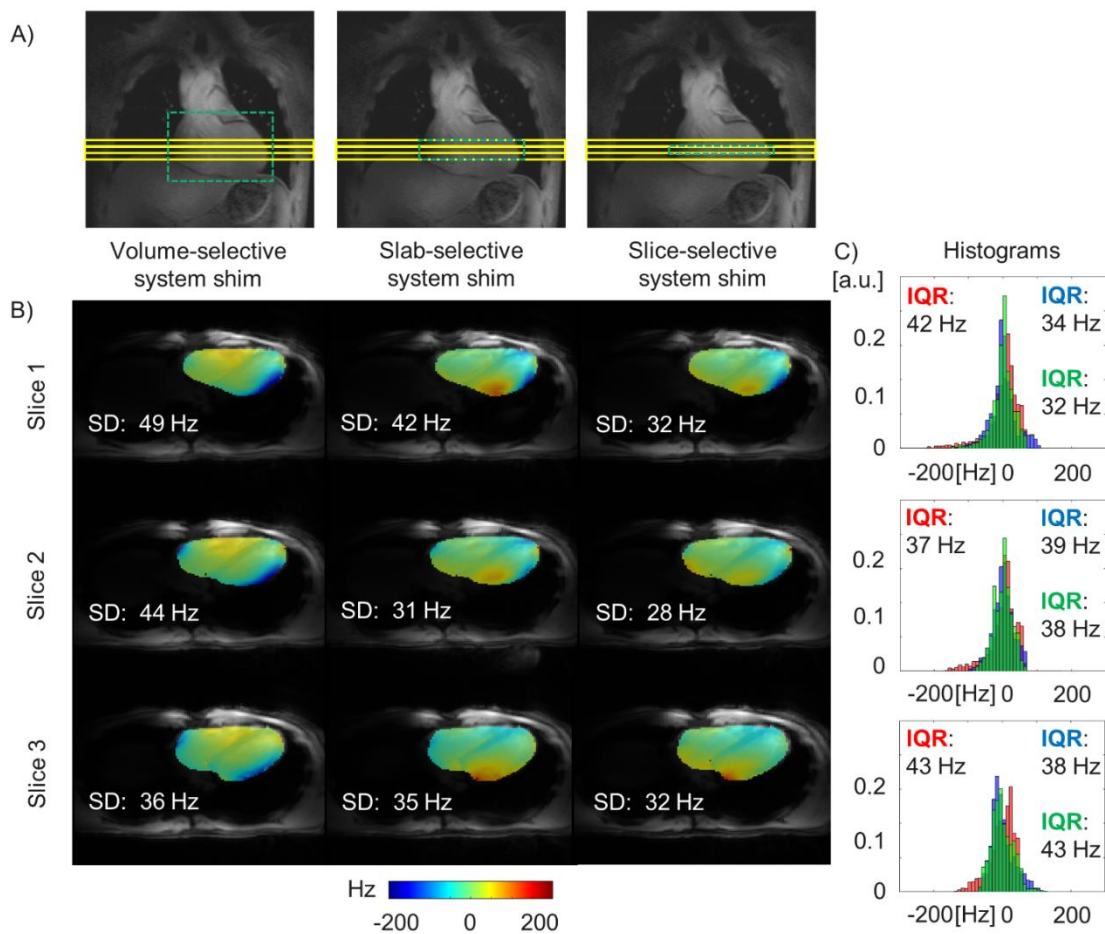


**Figure 12.** Temporal B<sub>0</sub>-field variation in the myocardium over the cardiac cycle. The left- (A) and right-ventricular myocardium (B) were opted for analog to Figure 11B and Figure 11H. The differences  $\Delta$ SD and  $\Delta$ IQR between B<sub>0</sub>-field distributions in (B), which were computed for the same systolic and diastolic cardiac phases as displayed in (A), are summarized for all study group subjects in box plots. Here, the red line markers delineate the median, and the blue line markers illustrate the 25<sup>th</sup> and 75<sup>th</sup> percentiles. The black line markers correspond to the most extreme data points not considered outliers, and outliers are visualized as a red '+'. Note that volume-selective shimming was performed prior to the B<sub>0</sub> map acquisition. Adapted from Reference (84).

## 4.2 Evaluation of heart-specific $B_0$ shim strategy

### 4.2.1 Shim-region-of-interest selection

After application of the volume-, slab-, and slice-selective shimming,  $B_0$  maps were acquired in each case to evaluate the three SROI selections (Figure 13).



**Figure 13.** Adjustment of the shim-region-of-interest (SROI). The adaption of the SROI cuboid is visualized for the vendor-supplied volume-, slab-, and slice-selective shimming (A). In each case, the SROI covered the entire heart, but as less parts of circumjacent organs as feasible in-plane. Exemplary, (B) shows the acquired  $B_0$  distribution for subject 7 in conjunction with the respective histograms in (C) gained after the volume- (red bins), slab- (blue), and slice-selective shimming (green). Adapted from Reference (84).

The slab-selective shimming led to a decreased SD and IQR in all three measured slices, implying a more homogeneous  $B_0$  distribution. Quantitatively, the slab-selective shimming reduced the SD of the  $B_0$  distribution in the central slices by  $13 \pm 6$  Hz and  $(26 \pm 11)$  % versus the volume-selective shimming across all study group subjects (Table 2). However, the insight delivered by Table 2 unveiled that slice-selective shimming reduced this value further for no more than two subjects.

**Table 2.** Comparison of different vendor-supplied shimming procedures. The field homogeneity is quantified by the standard deviations (SD) of  $B_0$  distributions at a mid-diastolic cardiac phase as exemplary demonstrated for subject 7 in Figure 13. Note that the SDs are provided for the central slices of the three-slice stack through the heart. The last row presents the mean value SD across all subjects

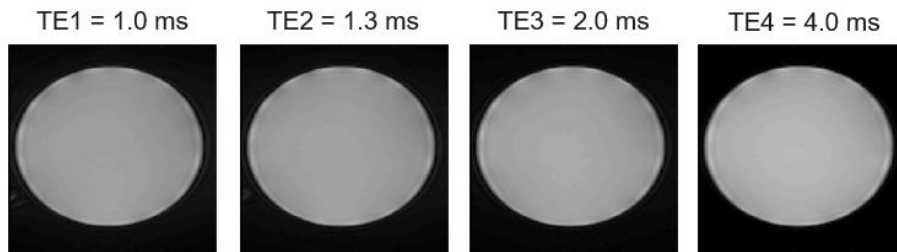
<b>Subject</b>	<b>Volume-selective shimming SD (Hz)</b>	<b>Slab-selective shimming SD (Hz)</b>	<b>Slice-selective shimming SD (Hz)</b>
5	42	32	39
6	49	28	54
7	44	31	28
8	66	46	42
9	49	45	49
10	51	39	45
	$50 \pm 8$	$37 \pm 7$	$43 \pm 8$

#### 4.2.2 Calibration of spherical harmonics shim system

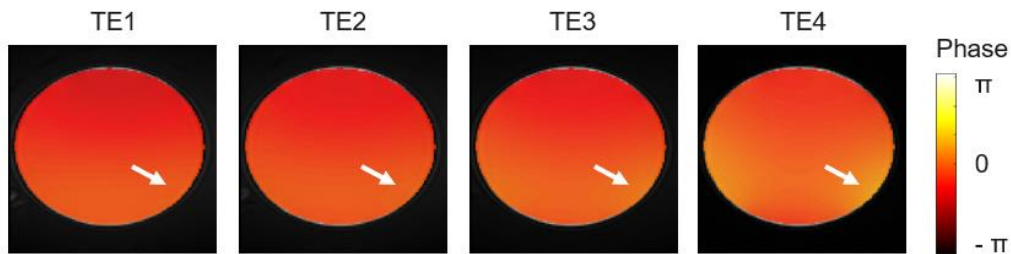
An individual step of appropriate  $B_0$  mapping of a certain underlying shim field is summarized in Figure 14 for the spherical oil phantom experiment. The static magnetic field reconstruction was based on linear regression of the signal phase evolution over four different TE values and computed voxel-by-voxel. The complete calibration routine for a specific shim component, which in this case was the SH term  $Z(X^2-Y^2)$ , is demonstrated in Figure 15. All corresponding generated cross-terms are given in Figure 16.

For all SH terms the entire calibration procedure visualized in Figure 15 and Figure 16 was repeated. The total dynamic range of each shim coil was:  $X = 2124$  Hz/cm,  $Y = 2120$  Hz/cm,  $Z = 2129$  Hz/cm,  $X^2-Y^2 = 6.1$  Hz/cm<sup>2</sup>,  $ZX = 12.6$  Hz/cm<sup>2</sup>,  $Z^2 = 40.2$  Hz/cm<sup>2</sup>,  $ZY = 12.3$  Hz/cm<sup>2</sup>,  $XY = 6.2$  Hz/cm<sup>2</sup>,  $Z(X^2-Y^2) = 0.10$  Hz/cm<sup>3</sup>,  $Z^2X = 0.35$  Hz/cm<sup>3</sup>,  $Z^3 = 0.68$  Hz/cm<sup>3</sup>,  $Z^2Y = 0.34$  Hz/cm<sup>3</sup>. Figure 17 provides the entire final calibration matrix. Note that the observed shim-to-shim interactions between 3<sup>rd</sup>- and 1<sup>st</sup>-order SH terms were eminent, whereas they were less prominent but still not negligible between 3<sup>rd</sup>- and 2<sup>nd</sup>-order as well as 2<sup>nd</sup>- and 1<sup>st</sup>-order terms.

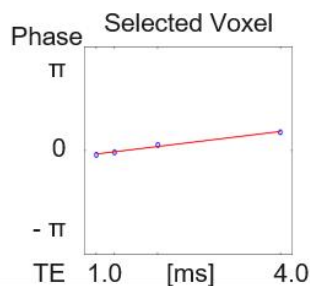
A) Magnitude images



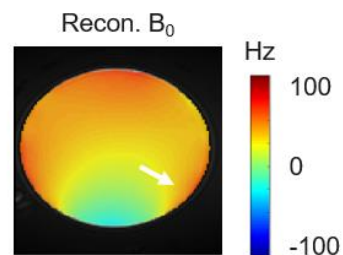
B) Signal phase-maps



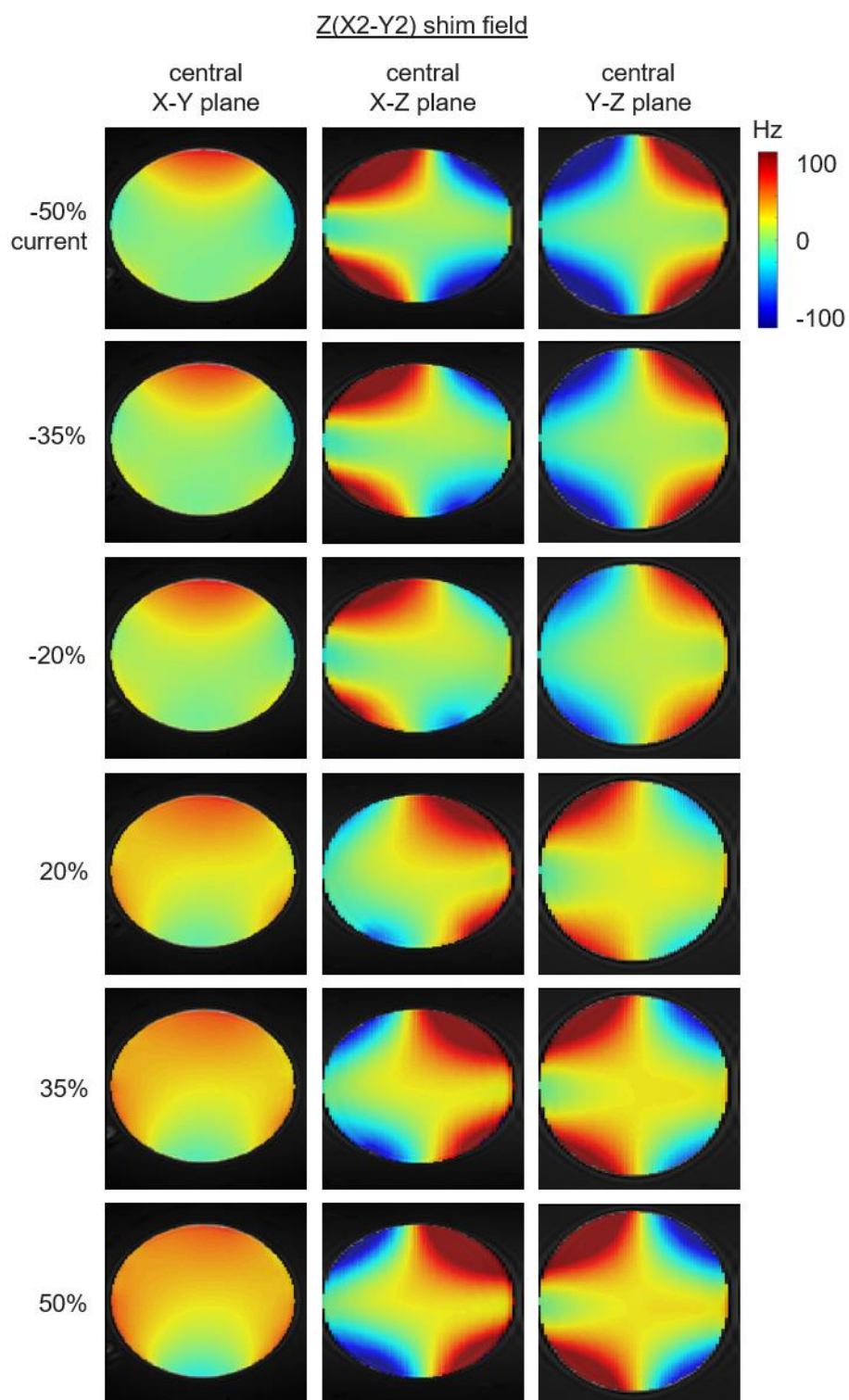
C) Voxel-wise linear regression



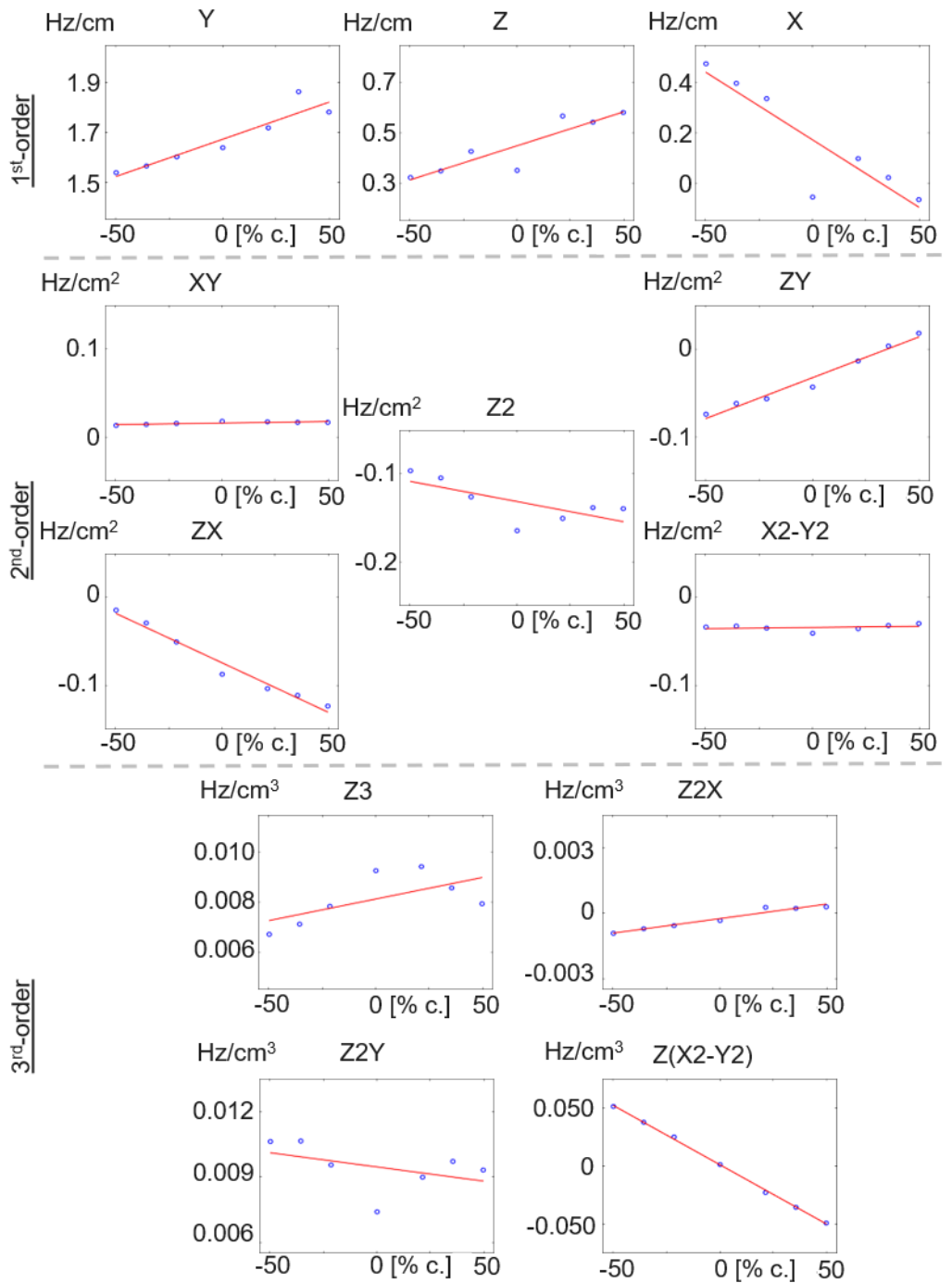
D) B<sub>0</sub>-field mapping



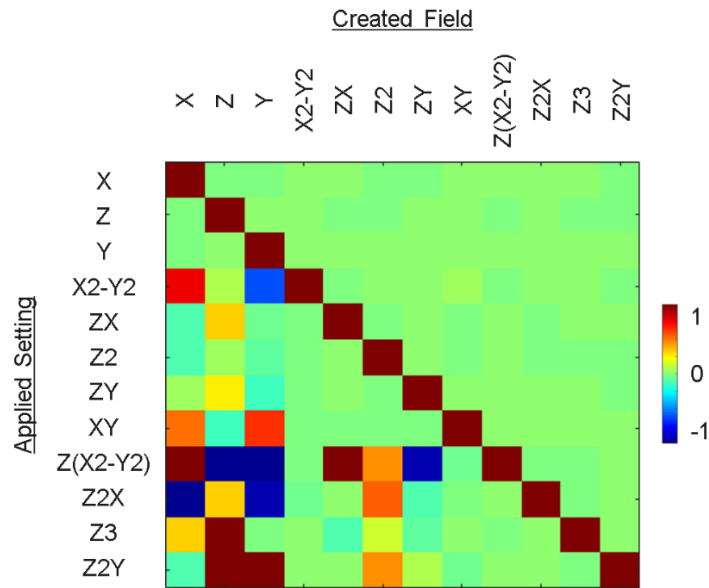
**Figure 14.** B<sub>0</sub> field mapping based on the phase evolution over multiple echo times (TE). Shown are the magnitude images (A) and signal phase-maps (B) acquired at four TE, as well as exemplary voxel-wise linear regression (C) and the reconstructed B<sub>0</sub>-field (D).



**Figure 15.** Calibration procedure for an individual spherical harmonics (SH) shim term. The current generating the 3<sup>rd</sup>-order SH term Z(X<sup>2</sup>-Y<sup>2</sup>) was varied in seven steps ranging from -50% to 50% of the shim coil's total dynamic range. Note that 0% is not shown.



**Figure 16.** Generation of self- and cross-terms through the calibration procedure. Shown are the self- and all cross-terms generated by varying the 3<sup>rd</sup>-order spherical harmonic (SH) term  $Z(X^2 - Y^2)$ . The shim current was changed in seven steps ranging from -50% to 50% of the maximum current, and the resulting shim fields are given in Hz/cm<sup>n</sup> (blue circles). Linear regression was performed to obtain the slope required for the calibration matrix (red lines). Note that present cross-terms were only derived for the scanner-integrated SH shim terms.



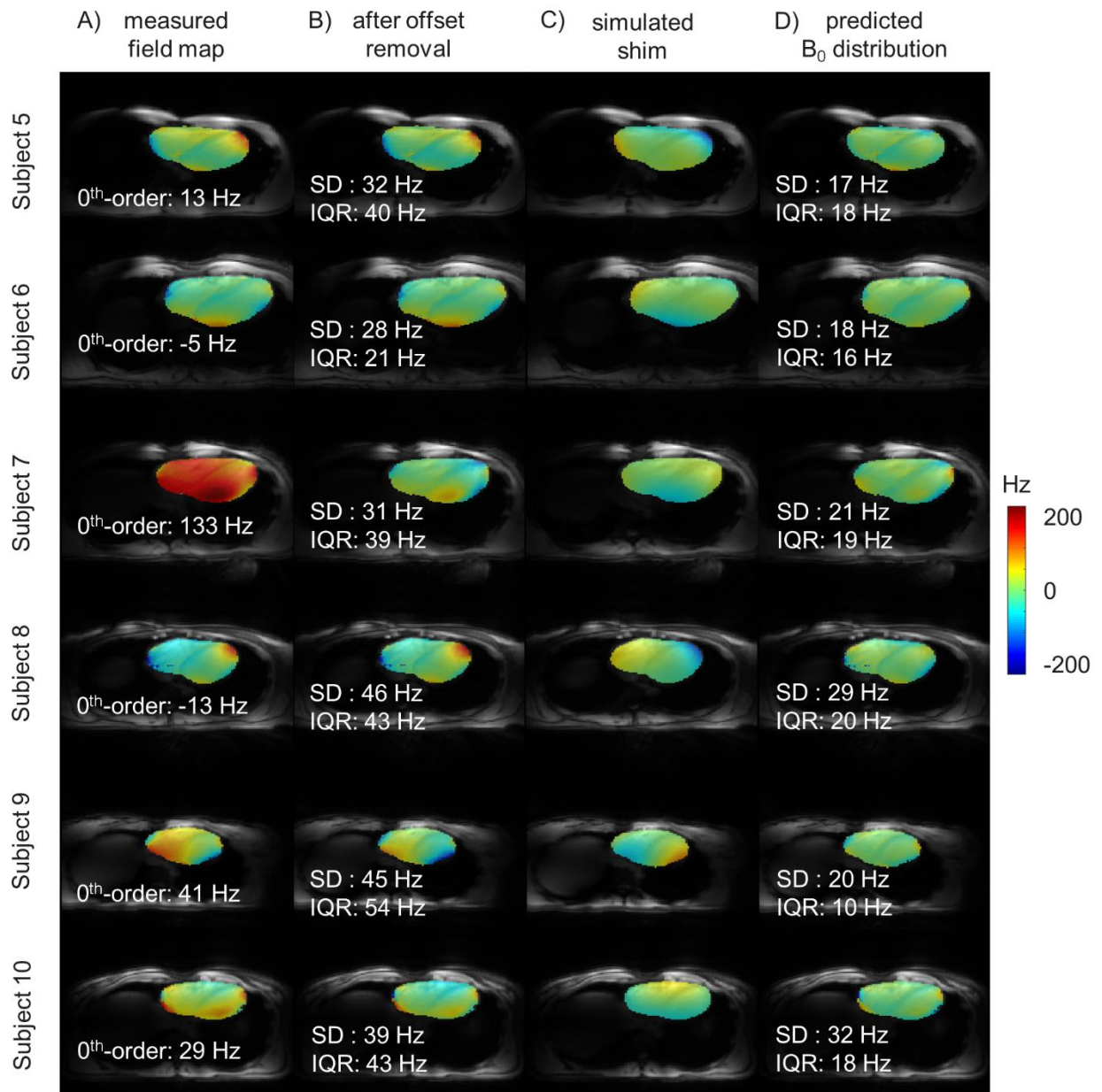
**Figure 17.** Calibration matrix for the partial 3<sup>rd</sup>-order SH shim system. The self-terms are displayed on the diagonal elements, and the cross-terms are located off-diagonal. In this case, the color encoding represents the normalized slopes.

#### 4.2.3 Simulation of static shimming

The  $B_0$  maps acquired after the slab-selective shimming unveiled the spatial field patterns inside the heart (Figure 18A and Figure 18B). Shim field simulations for the anatomy-matched SROIs, which were based on a calibration procedure as described in Section 2.4, led to predicted  $B_0$  distributions (Figure 18D). For the latter decreased SDs and IQRs occurred versus the measured  $B_0$  maps.

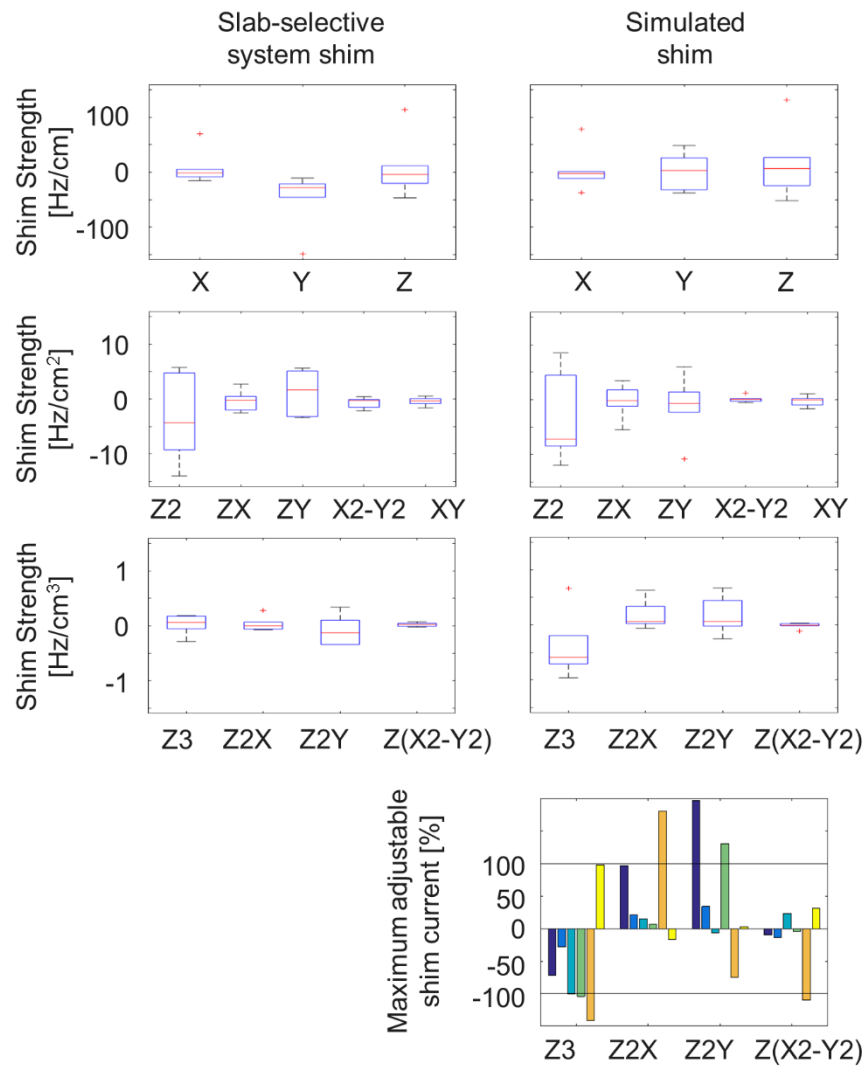
The shim field strengths for both the slab-selective shimming and the simulated shim (Figure 18C) were summarized in Figure 19. The medians of the X-, Y- and Z-gradient offsets differed just slightly (Figure 19, top row). Across all 3<sup>rd</sup>-order SH components, the zonal term Z3 featured the strongest difference. In four of the six subjects, the currents required for the simulated shim surpassed the hardware capabilities (Figure 19, bottom plot).



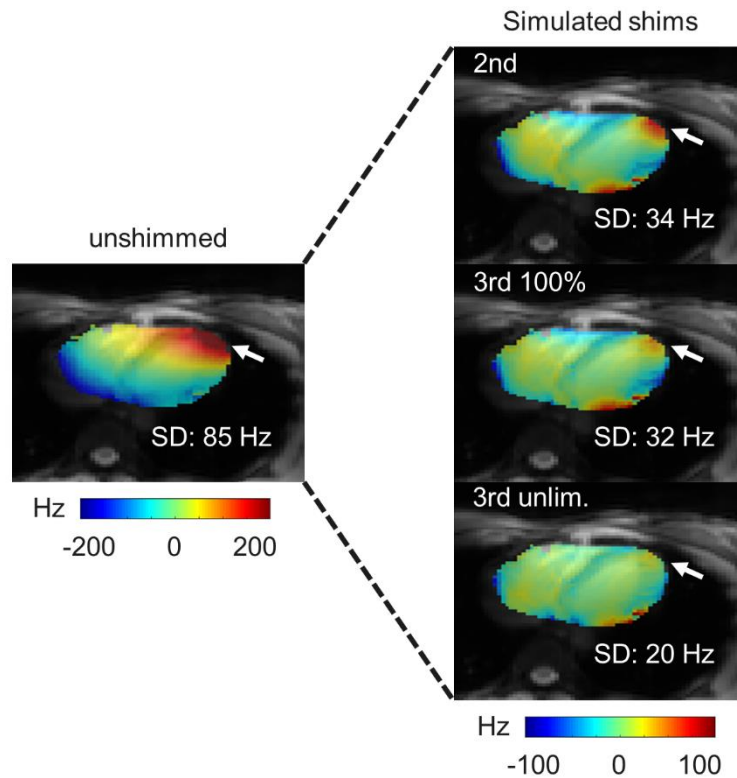


**Figure 18.** Calibration-based shim field simulations for an anatomy-matched SROI. The  $B_0$  distributions acquired after the slab-selective shimming as shown in Figure 13A are provided for the central slices with present center frequency offset (“measured field map”, A) and without (“after offset removal”, B). Additionally, the calibration-based computed shim fields (“simulated shim”, C) and the anticipated  $B_0$  distribution after their application (“predicted  $B_0$  distribution”, D) are shown. While A and B were obtained for a SROI cuboid, C and D were linked to the anatomy-matched SROI. Note that the scanner-integrated slab-selective shimming failed to correct the center frequency after modifying the higher-order shim field terms. This offset could be removed by adjusting the MR system’s resonance frequency. Adapted from Reference (84).

When shimming with up to 2<sup>nd</sup>-order SH terms was compared to shimming with inclusion of 3<sup>rd</sup>-order terms, the latter was advantageous to homogenize the B<sub>0</sub> field in the anterolateral segment of the left-ventricular myocardium (Figure 20). However, hardware restrictions of the scanner-integrated shim system led to remainders of the 3<sup>rd</sup>-order terms. No 2<sup>nd</sup>-order term surpassed the hardware restrictions for any shim.



**Figure 19.** Required shim field strengths for SH components employed by the slab-selective and simulated anatomy-matched shimming shown in Figure 18. The relevant 3<sup>rd</sup>-order terms are visualized at length for the simulated shim in the bottom, where each color stands for one subject. The hardware restrictions of the scanner-integrated shim system are delineated with black lines. Adapted from Reference (84).



**Figure 20.** Relevance of higher-order SH terms for  $B_0$  shimming of the heart. 3<sup>rd</sup>-order shimming was simulated with and without hardware restrictions. The un-shimmed  $B_0$ -field featured less than 5% of the maximum magnetic field strength feasible with each coil. Adapted from Reference (84).

#### 4.2.4 Simulation of dynamic shimming

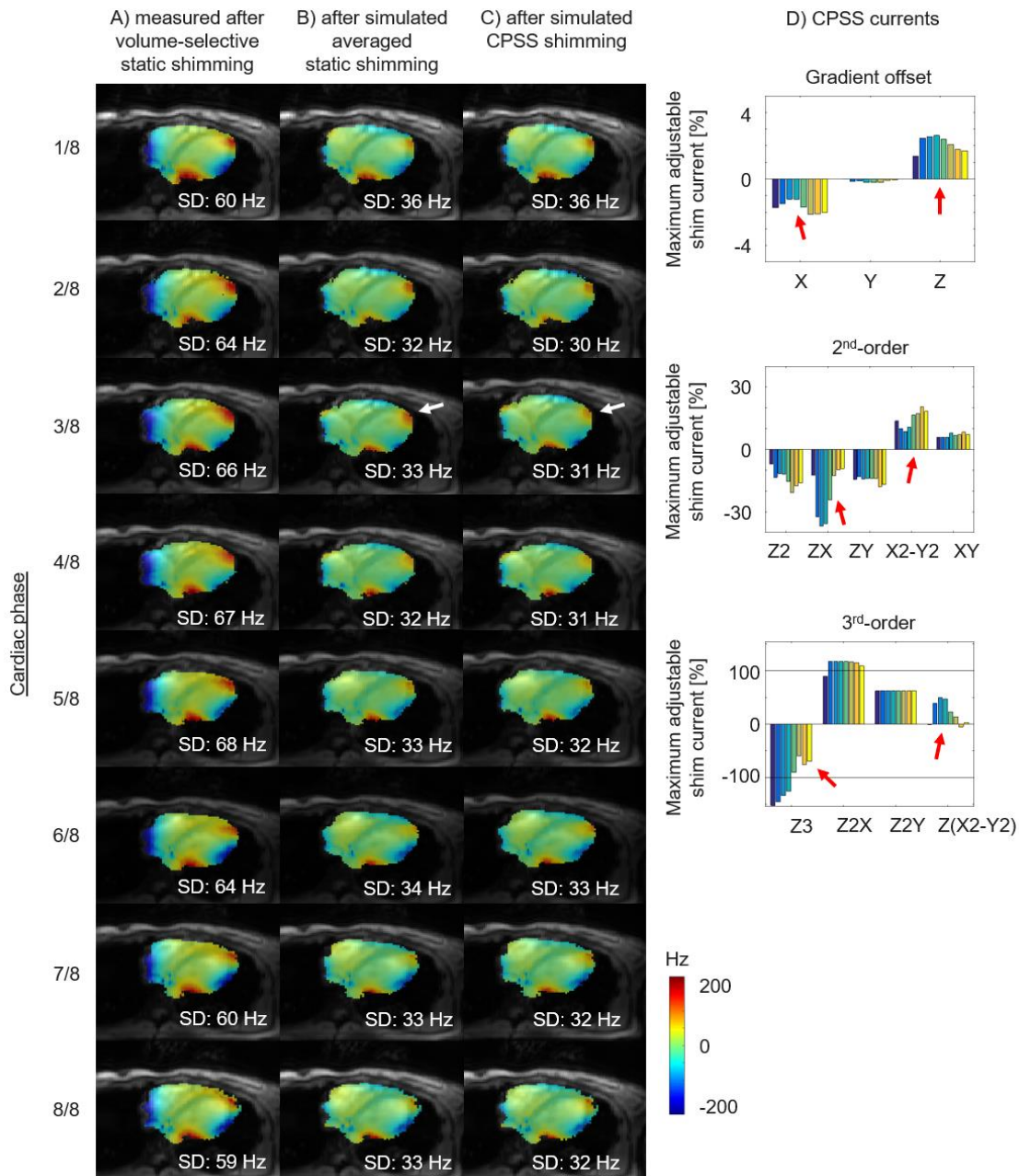
The temporal  $B_0$ -field fluctuations over the cardiac cycle, which occurred after volume-selective shimming, are summarized for the eight equally-spaced phases in Figure 21A. The application of two shimming approaches to the measured  $B_0$ -fields was simulated subsequently. The MR system employed in this study was not equipped with the hardware essential for CPSS, which consisted of the triggered  $B_0$  map acquisition, anatomy-matched selection of the shim-region-of-interest (SROI), and calibration-based  $B_0$  field modeling. Therefore, its simulation allowed to judge on whether the MR system should

be upgraded with the desired hardware, or an averaged static shim, which facilitated the mean of all eight CPSS fields, would be suitable for applications such as cine imaging instead. Averaged static shimming would lower these  $B_0$ -field inhomogeneities (Figure 21B). An even further reduction of myocardial  $B_0$ -field variations would be expected after simulated CPSS with anatomy-matched SROIs refreshed over the cardiac cycle (Figure 21C - cardiac phase 3, white arrow).

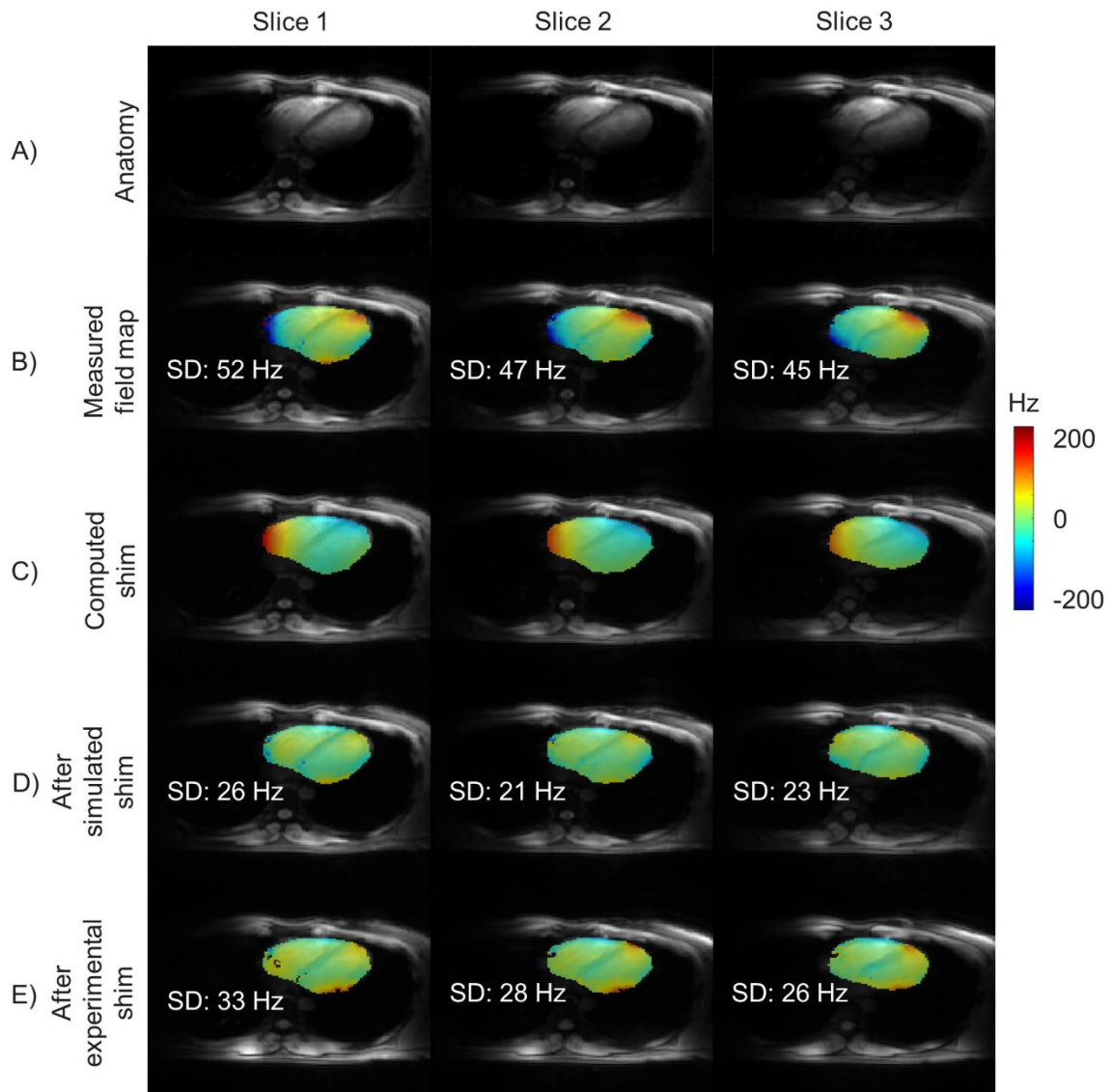
The optimal CPSS currents were found to alter in time over the cardiac cycle, which is highlighted for specific shim terms in Figure 21D (red arrows). Averaged over the six study group subjects, simulated CPSS resulted in a reduction of  $\Delta SD = 1 \pm 1$  Hz of the  $B_0$  distribution over the whole heart in contrast to averaged static shimming. In particular, CPSS was advantageous to lower myocardial  $B_0$ -field alterations, which is illustrated for subject 3 in Figure 21.

#### 4.2.5 Advanced in vivo $B_0$ shimming

Preliminary findings of the advanced in vivo  $B_0$  shimming are displayed in Figure 22. This heart-specific shim strategy included the triggered  $B_0$  map acquisition, anatomy-matched selection of the shim-region-of-interest (SROI), and calibration-based  $B_0$  field modeling. In the initial field maps, large  $B_0$  variations were present in both the left- and right-ventricular myocardium prior to the shim (Figure 22B). These  $B_0$ -field variations were estimated to decrease substantially by means of the advanced shim simulations (Figure 22D). The simulated shim result was in good agreement with the experimental shim result (Figure 22E), and lowered the SD within the SROI from 45-52 Hz to 26-33 Hz slice-to-slice. Admittedly, shallow  $B_0$ -field distortions persisted within the myocardium, which were most notable in the left ventricle.



**Figure 21.** Cardiac phase-specific shimming (CPSS) in the heart for subject 3. Next to the B<sub>0</sub> field in the central slice observed after volume-selective shimming (A), the estimated outcome after both averaged static shimming (B) and CPSS (C) is demonstrated. The currents required to realize CPSS are given in (D), where each cardiac phase is illustrated by a different color. The averaged static shimming is characterized by using the mean shim field of all CPSS settings. Taking all six subjects of the study group into account, the standard deviation of the B<sub>0</sub> field distribution over the whole heart was reduced by  $\Delta\text{SD} = 1 \pm 1$  Hz in contrast to averaged static shimming. Adapted from Reference (84).



**Figure 22.** Initial in vivo results of 3<sup>rd</sup>-order  $B_0$  shimming with the advanced shim strategy for subject 12. The magnitude images were used to extract the anatomy-matched SROI (A). Beside the primary measured  $B_0$ -field distributions (B) the correcting magnetic fields, which were computed via the advanced shim strategy (C), are visualized. The  $B_0$ -field distributions anticipated after the advanced shim (D) and measured after its experimental application (E) largely concurred. It has to be mentioned that the center frequency was subtracted from all field maps. Adapted from Reference (84).

## 5 Discussion

The accurate measurement and quantification of the myocardial  $B_0$ -field variations at 7 T in terms of both their spatial distribution and fluctuation over the cardiac cycle were analyzed in this work. High off-resonances appeared in localized spots, while temporal perturbations were observed between different cardiac phases. To reduce these  $B_0$  inhomogeneities, three key factors were identified to be crucial and led to an advanced shim strategy: the triggered  $B_0$ -map acquisition, the anatomy-matched SROI selection, and calibration-based  $B_0$ -field modeling in dedicated shim software. Simulations of static shimming, which took these aspects into account, allowed to investigate the technical requirements for the employed shim system. The 3<sup>rd</sup>-order SH terms proved to be beneficial for  $B_0$ -field homogenization in comparison to the standard approach, which only uses the 2<sup>nd</sup>-order terms. The optimal shim currents, however, exceeded the capabilities of the built-in shim amplifiers in several cases. Simulations of dynamic shimming enabled insights into the potential advantages of CPSS. When the required shim field was calculated for different heart phases, monitoring of the individual required shim terms over the cardiac cycle unveiled oscillations. Initial in vivo results of the implemented advanced shim strategy widely matched the simulations.

### 5.1.1 Myocardial $B_0$ -field inhomogeneities

In the presented work increased spatial  $B_0$ -field distortions were observed in the myocardium, which showed good agreement with previous studies (7,19). Their source was investigated with high-resolution simulations of the  $B_0$ -field conditions in the heart, which besides revealed that the positions of common  $B_0$ -field variations and dark band artifacts concur (85). Across the cardiac cycle, the  $B_0$  distribution in the myocardium of both ventricles varied over time. This finding coincides with previous investigations, which explored the relationship between wall thickness and  $T_2^*$  of the left-ventricular myocardium (86-88). The temporal  $B_0$  field fluctuations over the cardiac cycle substantiate the integration of a triggered pulse sequence into the shimming workflow. In this context, the diastolic SD of  $B_0$  was not found to always being smaller than the systolic

SD across all subjects. A reason for this fact might be the transversal orientation of the  $B_0$  field maps, which implicated highly subject-specific views. For SA or LA image orientations, either the SD at systolic or diastolic cardiac phases might always be lower, and this issue remains to be inspected when the shim strategy will be adjusted to anatomical views.

Data acquisition which lasts over several breath-holds could also lead to significant respiration-induced  $B_0$  field variations. These variations could be analyzed by multiple repetitions of a scan over consecutive breath-holds. A previous examination demonstrated that local  $B_0$  fluctuations accounted for 100 Hz and beyond, although their mean value varied only modestly between inhaled, half-exhaled, and exhaled breath-hold positions (11). To split the acquisition of multiple slices over repeated breath-holds, the  $B_0$  maps may prospectively be measured together with diaphragm navigator images. The respiratory position would then be revealed during a calibration scan and a suitable correction could be employed. Monitoring of  $B_0$  fluctuations with field probes and real-time  $B_0$  field updating with a dynamic shim module could be an additional solution, which was proven to minimize respiration-induced  $B_0$  field variations in the chest at 7 T (89).

### 5.1.2 Requirements for static shimming

Contrary to the volume-selective approach, the slab-selective shimming decreased these  $B_0$  field variations in the heart considerably. The latter method made use of a SROI cuboid which had the same height as the three acquired slices, i.e., 18 mm, and was adjusted to accurately cover the whole heart in-plane. The slice-selective shimming, which employed a SROI capturing the central slice in height but an equal area in-plane, caused no additional decrease of the SD in 4 of the 6 subjects. Indeed, straight transversal slice orientations might promote partial volume effects (90). In addition, the slice-selective shim results were potentially affected by physiological alterations between the measurement of the first  $B_0$  map applied for the shim current calculation and the second for the shim evaluation. If so, the 3D  $B_0$  map should capture a SROI more than one slice thickness wider in both directions for a dependable shim. In-plane shim field simulations for an anatomy-matched SROI, which were expected to lower the  $B_0$  field distortions



further in comparison with cuboid-based slab-selective shimming, are discussed further down the line.

Localized spots of minor  $B_0$  field variations persisted in the myocardium despite advanced partial 3<sup>rd</sup>-order SH shimming for an anatomy-matched SROI. These residual alterations might be a consequence of the shim system's hardware restrictions, which would not always be capable of realizing the subject-specific shims as desired. Considering that the  $B_0$ -field inhomogeneities localized in small regions, the hardware capabilities of the scanner-integrated partial 3<sup>rd</sup>-order shim system might not impair cine imaging and consequent myocardial contour-tracking to estimate volumetric parameters and cardiac function. However, the characterization of tissue microstructure by quantitative MRI methods such as pixel-wise  $T_2^*$  mapping could profit more from improved hardware capabilities of the shim system. In this case, the relaxation time computation could become inaccurate when disease-affected tissue, e.g., a scar resulting from myocardial infarction, and areas of strong  $B_0$  field-related off-resonances overlap. Another considerable factor could be the incidence of higher-order  $B_0$  field constituents such as the 3<sup>rd</sup>-order SH terms X3, Y3, and XYZ, which the vendor-supplied set of shim coils did not incorporate. The extensive shimming capabilities required to tackle these  $B_0$  field residuals might be realized by dedicated shim coil methodologies such as DYNAMITE (25,26), AC/DC (64), or iPRES (65). Various body shapes would complicate the arrangement of shim coils in the same localized setup for all experiments in comparison with brain applications, but could open exciting possibilities for future studies.

### 5.1.3 Potential of dynamic shimming

The advanced shimming methodology, which was developed within the scope of this work, was capable of performing a static shim designed for a certain cardiac phase or in an averaged fashion. To minimize  $B_0$ -field alterations over the cardiac cycle, CPSS was proven to enhance SSFP cine imaging at 3 T in a previous investigation (91). On the basis of these findings, the shim currents would ideally be adapted to each cardiac phase prospectively for cine imaging. Admittedly, the MR system at hand with its implemented

hardware did not enable dynamic shim updating, which would demand pre-emphasis and  $B_0$  compensation with a dynamic shim interface together with specific shim amplifiers for a fast adjustment of shim currents (30). Brief updating times for the electronic components could then be ensured by storing the CPSS settings at the local hardware memory of the dynamic shim interface. In a similar way, slab-wise dynamic shim updating would be another concept to enhance  $B_0$ -field homogeneity beyond static shimming for a stack of multiple slices (8). Initially, dynamic shim updating was demonstrated slice-wise in the human brain (27,92).

In cases where the implemented hardware prevents the use of CPSS, the averaged static shimming would be an adequate approach. By tracking the temporal  $B_0$ -field alterations in conjunction with required CPSS currents, the mean of all CPSS shim fields could be derived. The impact of CPSS on SSFP cine imaging could be examined by subsequent repetitions of the experiment with dedicated trigger delays and shim settings for individual cardiac phases, thus avoiding the practical implementation of dynamic shim updating. Since the observed  $B_0$  fluctuations were focused on smaller localized spots, the averaged static shimming might provide field homogeneity sufficient for deriving cardiac function and volumetric parameters from the myocardial contours determined via cine imaging. Quantitative MRI methods which evaluate the tissue microstructure on a pixel basis, in particular  $T_2^*$  mapping, could benefit the most from CPSS. Here, the localized spots of high  $B_0$ -field inhomogeneities and disease-affected tissue, e.g., a scar resulting from myocardial infarction, could coincide and have a severe impact on the relaxation time calculation. The advantage of CPSS for double-oblique image orientations remained to be proven, which is an important aspect for CMR applications and calls for an iteration of the analysis when this advanced shimming methodology would be aligned with the anatomical SA and LA views.

#### 5.1.4 Adaptation to clinical imaging

The missing potential of the presented advanced shim strategy to homogenize the  $B_0$  field for the double-oblique anatomical SA and LA image orientations was a drawback and impaired its adaptation to clinical CMR imaging. A possible solution for this issue would

be a modification of the geometric formalism of characterizing image rotations by two Euler angles, which has been proven to be suitable for shimming of single-oblique slices in the brain (93). In this context, the efficiency of the 3<sup>rd</sup>-order SH terms remained to be proven for varying image orientations in comparison with the transversal slice geometries. As a result, technical demands for the shim coils might vary. Alternatively, a stack of transversal slices could be positioned so as to contain the fraction of the heart region relevant for the anatomical views. A slice-wise anatomy-matched SROI selection in conjunction with a sufficient number of slices would allow shimming based on transversal field map data. Increased slice resolution and, therefore, measurement time would be required to minimize partial volume effects (90).

Slice-wise as well as cardiac phase-specific SROI segmentations were time-consuming when performed manually. To automate the segmentation process, deep learning (DL) approaches have been beneficial (94). Here, a sensitivity analysis would be a suitable approach to determine whether a DL-based segmentation model trained on a specific data set acquired at a certain field strength and with certain imaging parameters could provide accurate segmentation on another data set at which these parameters vary (95). Initial results produced by the employed software package in a dedicated case study were promising, however, the amount of training data in terms of  $B_0$  field maps must be increased to achieve meaningful model predictions across large-scale subject cohorts.

Furthermore, whole-heart volume-selective shimming was also reported in detail for a large-scale study of 84 examinations, and two notable observations attracted attention (96). Firstly, the available 3<sup>rd</sup>-order SH shim coils were strongly employed across all subjects. Secondly, the Z3 shim term was used to capacity for numerous subjects. To avoid the permanent running of shim coils at capacity and the risk of hardware damaging, there would be potential to further improve passive shimming, i.e., ferromagnetic shim elements (97), for CMR imaging at 7 T. Beside the different inter-subject  $B_0$ -field conditions, inter-site variations could also be investigated for the heart similar as for the brain (98).

### 5.1.5 Implications for MR methods development

When it came to the accuracy of shim field computations, the resolution of the measured  $B_0$  distribution played an important role. Here, SH terms like X<sup>2</sup>-Y<sup>2</sup> or XY with an eminent dependency on the in-plane  $B_0$  field were resolved in detail with the applied sequence parameters. In contrast, the SH terms like Z<sup>3</sup> with a substantial influence on the  $B_0$  field in z-direction were derived from through-slice data on the basis of the transversal 3D  $B_0$  maps. More accurate magnetic field modeling might be achieved by increasing the number of slices, which was confined to three within a single breath-hold up-to-date.

Improved precision in  $B_0$  field monitoring might also be reached by using a dynamic field camera, which would allow to correct  $B_0$  field-related errors in pulse sequences (37). This concept would also be capable of tracking spatio-temporal  $B_0$ -field fluctuations in the human heart at 7 T and their relationship to physiological processes (99). To increase the spatial resolution of the  $B_0$ -field maps as the basis for shim computations, the field probe approach might be applied in conjunction with advanced cardiac shim strategies in the future. In addition, the dynamic field camera could be employed to track  $B_0$ -field variations during dynamic shimming on multiple slices. Here, periodical fluctuations were reported across the SH terms and demanded a pre-emphasis of the applied dynamic shim fields. The pre-emphasis would have to take all shim-to-shim interactions into account and could be accomplished via impulse response functions, which were shown to enable the appropriate correction of gradients and shims (39,40).

Recently, pre-emphasis of the gradient impulse response function was also integrated into cardiac real time imaging at 7 T (47). In contrast to the promising imaging quality of measurements conducted at 3 T (33), blurring due to an inhomogeneous  $B_0$ -field occurred within the myocardium. Since the vendor-supplied shimming workflow was applied for field homogenization, higher  $B_0$ -related off-resonances persisted in the images (84). Their correction would be feasible in two ways. On the one hand, the post-processing procedure for the acquired image data could take the underlying  $B_0$ -field into account. While a constant 0<sup>th</sup>-order frequency offset across the FOV resulted in considerable blurring removal, additional improvement could be expected from techniques which consider the complex spatial  $B_0$ -field distribution across the human heart (100-104). On the other

hand, the advanced shim strategy presented in this work could assess the myocardial  $B_0$ -field fluctuations before the actual data acquisition (84). Both approaches would ideally be combined for effective blurring removal.

#### 5.1.6 Overall discussion

The quantification of  $B_0$ -field inhomogeneities in the human heart and their correction, i.e.,  $B_0$  shimming, could be compared to several studies conducted at a magnetic field strength of 3 T. In the context of simultaneous  $B_0$ - and  $B_1^+$ -map acquisition for fast localized shim, frequency, and RF power determination in the heart at 3 T (77), dual TE  $B_0$ -mapping techniques were used to measure multi-slice field maps covering the  $B_0$ -field distribution across the entire heart in a single breath hold and eighteen cardiac cycles. Heart-specific 2<sup>nd</sup>-order shimming, which also incorporated the 0<sup>th</sup>-order  $B_0$  offset correction, was conducted in seven healthy adult human subjects and improved the SD of the acquired  $B_0$  field from 60 Hz to 35 Hz in comparison to an automated 1<sup>st</sup>-order shimming routine.

Even at a magnetic field strength of 3 T, it was demonstrated that the use of SSFP-based pulse sequences for CMR is negatively affected by  $B_0$ -field imperfections inside the heart (91). To quantify temporal  $B_0$ -field variations across heart phases,  $B_0$ -field maps were acquired at multiple phases of the cardiac cycle. For 1<sup>st</sup>- and 2<sup>nd</sup>-order SH shimming, cardiac phase-specific shim settings were derived and evaluated both in simulation and in vivo. Within the entire heart, a mean variation of the SD of approximately 10 Hz was observed across twenty volunteers. Moreover, it was demonstrated that an anatomy-matched SROI is advantageous for accurate  $B_0$ -shimming of the heart, which could be seen from a reduction of field inhomogeneity by 32% when applying heart-specific 2<sup>nd</sup>-order  $B_0$ -shimming in comparison to a standard SROI cuboid. Beyond, 2<sup>nd</sup>-order CPSS lead to an additional improvement of 39%.

An approach combining active and passive shimming was evaluated by examining the effect of high-permittivity pads on specific absorption rate in RF- or  $B_1^+$ -shimmed dual-transmit cardiovascular magnetic resonance at 3T (105). Together, active  $B_1^+$  shimming

in the form of dual transmit, and passive  $B_1^+$  shimming, i.e., high permittivity pads, resulted in improved image quality in CMR at 3 T due to optimized  $B_1^+$  homogeneity.

At the initial in vivo application of the advanced  $B_0$  shimming strategy developed in this study, experimentally measured after-shim  $B_0$ -field agreed well with the simulated after-shim  $B_0$ -field. Concededly, marginal  $B_0$ -inhomogeneities remained within the myocardium, which were most remarkable in the left ventricle. It has to be noted that the period of time between the acquisition of the first  $B_0$ -map, which the shim computation was based on, and the second one, which measured the  $B_0$ -field after the experimental shim served, accounted for approximately one hour. While the same trigger delay was employed for both measurements, the volunteer's heart rate and, subsequently, the duration of the overall cardiac cycle could have changed over this period of time. Triggering the pulse sequence at a different time spot of the cardiac cycle would then result in a residual  $B_0$ -field due to the temporal  $B_0$ -field variations in the myocardium, which were explained previously. Therefore, it has to be ensured in the future that the trigger delay is adjusted for measuring the validation  $B_0$ -map to match the same time spot in the cardiac cycle as for measuring the initial  $B_0$ -field before shimming.

Further in vivo application of the advanced  $B_0$  shimming strategy was prevented by spatial phase-wrapping in the measured  $B_0$ -field maps. The spatial phase-wrapping lead to leaps of the signal phase from positive to negative phase values and vice versa. As a result, physically not plausible leaps of the  $B_0$ -field occurred and could not be corrected for. Throughout this study, the spatial phase-unwrapping algorithm PRELUDE of the FSL (57,75) was employed. To improve the phase-unwrapping capabilities of the presented workflow, additional algorithms could be implemented and compared in the future. One option could be the rapid open-source minimum spanning tree algorithm (*ROMEO*) (58), which offers and improved phase-unwrapping paths and could as well perform single-step unwrapping across a fourth dimension to enable temporal phase unwrapping across the different TE for  $B_0$  mapping.

## 6 Conclusion and Outlook

This work addressed the development of advanced shimming techniques for CMR to correct the spatio-temporal  $B_0$  field variations present in the human heart at 7 T. State-of-the-art CPSS, which facilitated the triggered  $B_0$  map acquisition, anatomy-matched SROI selection, and calibration-based SH field modeling, outperformed standard vendor-supplied shimming. These technical improvements are summarized hereafter.

The spatial pattern of the  $B_0$ -field within the human heart was found to be non-isotropic, while strong inhomogeneities occurred within the myocardium. Particularly these spots showed temporal fluctuations when monitored over multiple cardiac phases and gave rise to the embedding of a triggered  $B_0$ -mapping pulse sequence into the shimming procedure. A detailed decomposition of the spatial  $B_0$ -field distribution into SH constituents, in which shim-to-shim interactions were accounted for via a calibration process, revealed the benefit of higher-order correcting magnetic fields. To remove certain third-order components completely, either the passive shimming of the magnet could be tailored to CMR applications, or the amplifiers of the shim coils could be upgraded. The development of dedicated multi-coil shimming technology adapted to the human body could also address this challenge. While a precise SROI labeling was demonstrated to be essential for  $B_0$ -field homogenization, it remained a time-consuming work step and should in the future be addressed by transfer learning approaches using DL-based automated segmentation models to leverage advanced  $B_0$  shimming. The first in vivo application of this shim strategy led to promising results for a healthy volunteer, for which the  $B_0$  field measured after shimming was in good agreement with the simulated one. To unleash the full potential of this technique to clinical imaging, the possibility to compute shim fields for double-oblique slice orientations, i.e., the anatomical SA and LA views, would be a prerequisite. Furthermore, certain techniques for tissue characterization, e.g., temporally resolved  $T_2^*$  mapping, might profit by CPSS. Dynamic shimming on multiple cardiac phases, which ranged from systole to diastole, would result in reduced  $B_0$ -field inhomogeneities as proven by simulations. When the required hardware is not available, the varying shim fields, which oscillate over the cardiac cycle, could be assessed by a static shim which averages the cardiac phase-specific settings.

The presented technical developments showcase significant improvements on the way to quantitative cardiac magnetic resonance imaging of the human heart at ultra-high field strength. Together with other potential innovations, e.g., applications of the dynamic multi-coil technique, clinical studies about cardiac diseases seem in reach soon.



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# Publications

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$B_0$  shimming of the human heart at 7T.

*Magn Reson in Med* 2021; 85:182-196, DOI: 10.1002/mrm.28423.

Ankenbrand MJ, Shainberg L, **Hock M**, Lohr D, Schreiber LM.

Sensitivity Analysis for Interpretation of Machine Learning Based Segmentation Models in Cardiac MRI.

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Voelker MN, Kraff O, Goerke S, Laun FB, Hanspach J, Pine KJ, Ehses P, Zaiss M, Liebert A, Straub S, Eckstein K, Robinson SD, Nagel AM, Stefanescu MR, Wollrab A, Klix S, Felder J, **Hock M**, Bosch D, Weiskopf N, Speck O, Ladd ME, Quick HH.

The Traveling Heads 2.0: Multicenter Reproducibility of Quantitative Imaging Methods at 7 Tesla.

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Reiter T, Lohr D, **Hock M**, Ankenbrand MJ, Stefanescu MR, Kosmala A, Kaspar M, Juchem C, Terekhov M, Schreiber LM.

On the way to routine cardiac MRI at 7 Tesla – a pilot study on consecutive 84 examinations.

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Elabyad IA, Terekhov M, Lohr D, Bille M, **Hock M**, Schreiber LM.

A Novel Antisymmetric 16-Element Transceiver Dipole Antenna Array for Parallel Transmit Cardiac MRI in Pigs at 7T.

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## Conference Proceedings

### Conference contributions as first-author:

**Hock M**, Terekhov M, Ankenbrand M, Lohr D, Reiter T, Juchem C, Schreiber LM.  
Considerations for cardiac phase-specific  $B_0$ -shimming at 7 T.  
ISMRM 28<sup>th</sup> Annual Meeting & Exhibition, Virtual Conference & Exhibition, Abstract #1277 (Talk)

**Hock M**, Terekhov M, Reiter T, Lohr D, Juchem C, Schreiber LM.  
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2019 Minnesota Workshop on High and Ultra-high Field Imaging, Minneapolis, MN, USA (Talk)

**Hock M**, Terekhov M, Stefanescu M, Lohr D, Herz S, Juchem C, Schreiber LM.  
Reduzierung von lokalen  $B_0$ -Inhomogenitäten in der kardialen MRT bei 7 T durch Shimming der dritten Ordnung.  
50. Jahrestagung der Deutschen Gesellschaft für Medizinische Physik, Stuttgart, Deutschland (Traditional Poster)

**Hock M**, Stefanescu M, Terekhov M, Lohr D, Herz S, Juchem C, Schreiber LM.  
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**Hock M**, Terekhov M, Lohr D, Stefanescu M, Schroeder A, Walles H, Juchem C, Schreiber LM. Calibration of Siemens MAGNETOM<sup>TM</sup> Terra 7T Shim System and Analysis of Static 3<sup>rd</sup>-order  $B_0$ -Shimming of the Heart Using BODETOX.  
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ISMRM 29<sup>th</sup> Annual Meeting & Exhibition, Virtual Conference & Exhibition, Abstract #0021 (Digital Poster)

Lohr D, Bille B, Terekhov M, **Hock M**, Elabyad IA, Baltes S, Kollmann A, Reiter T, Schnitter F, Bauer WR, Hofmann U, Schreiber LM.  
Ultrahigh Field Cardiac MRI in a Large Animal Model of Acute and Chronic Infarction.  
ISMRM 29<sup>th</sup> Annual Meeting & Exhibition, Virtual Conference & Exhibition, Abstract #0960 (Digital Poster)

Terekhov M, Reiter T, **Hock M**, Lohr D, Bauer WR, Schreiber LM.  
Towards Clinical Application of the  $T_2^*$  quantification in the 7T Cardiac MRI: Reproducibility Study in Healthy Volunteers.  
ISMRM 29<sup>th</sup> Annual Meeting & Exhibition, Virtual Conference & Exhibition, Abstract #0984 (Digital Poster)

Elabyad IA, Terekhov M, **Hock M**, Lohr D, Schreiber LM.  
Development of a Dedicated Mono-surface 16-Element Transceiver Dipole Antenna Array for Parallel Transmission Cardiac MRI in Pigs at 7 Tesla.  
ISMRM 29<sup>th</sup> Annual Meeting & Exhibition, Virtual Conference & Exhibition, Abstract #1577 (Digital Poster)

Terekhov M, Lohr D, Reiter T, Elabyad IA, **Hock M**, Schreiber LM.  
New commercial 8Tx/16Rx array for Clinical 7T Cardiac MRI: initial experience.  
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Ankenbrand MJ, Shainberg L, **Hock M**, Lohr D, Schreiber LM.  
Sensitivity of a Deep Learning Model for Multi-Sequence Cardiac Pathology  
Segmentation to Input Data Transformations.  
ISMRM 29<sup>th</sup> Annual Meeting & Exhibition, Virtual Conference & Exhibition,  
Abstract #2652 (Digital Poster)

Reiter T, Lohr D, **Hock M**, Ankenbrand MJ, Stefanescu MR, Terekhov M, Schreiber  
LM.  
On the way to routine cardiac MRI at 7Tesla- using what we have.  
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Abstract #4295 (Digital Poster)

Stefanescu MR, Terekhov M, Elabyad IA, Lohr D, **Hock M**, Schreiber LM.  
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MRI at 7T.  
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Abstract #2151 (Digital Poster)

Lohr D, Terekhov M, Kosmala A, Stefanescu MR, **Hock M**, Schreiber LM.  
Cardiac MRI with the Siemens Terra 7T System: Initial Experience and Optimization of  
Default Protocols.  
ISMRM 26<sup>th</sup> Annual Meeting & Exhibition, Virtual Conference & Exhibition,  
Abstract #3014 (Traditional Poster)

## Affidavit

### Affidavit

I hereby confirm that my thesis entitled *Methods for Homogenization of Spatio-Temporal  $B_0$  Magnetic Field Variations in Cardiac MRI at Ultra-High Field Strength* is the result of my own work. I did not receive any help or support from commercial consultants. All sources and / or materials applied are listed and specified in the thesis.

Furthermore, I confirm that this thesis has not yet been submitted as part of another examination process neither in identical nor similar form.

Würzburg, March 17<sup>th</sup> 2023

Michael Hock, M.Sc.

### Eidesstattliche Erklärung

Hiermit erkläre ich an Eides statt, die Dissertation *Methoden zur Homogenisierung räumlicher und zeitlicher Variationen des  $B_0$ -Feldes in der kardialen Ultrahochfeld-MRT* eigenständig, d.h. insbesondere selbständig und ohne Hilfe eines kommerziellen Promotionsberaters, angefertigt und keine anderen als die von mir angegebenen Quellen und Hilfsmittel verwendet zu haben.

Ich erkläre außerdem, dass die Dissertation weder in gleicher noch in anderer Form bereits in einem anderen Prüfungsverfahren vorgelegen hat.

Würzburg, March 17<sup>th</sup> 2023

Michael Hock, M.Sc.



# Curriculum Vitae





