Non-Cartesian Parallel Magnetic Resonance Imaging

Dissertation zur Erlangung des naturwissenschaftlichen Doktorgrades
der Bayerischen Julius-Maximilians-Universität Würzburg

vorgelegt von
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Würzburg 2007
Eingereicht am:
bei der Fakultät für Physik und Astronomie

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Tag des Promotionskolloquiums:

Doktorurkunde ausgehändigt am:
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1 Introduction

In 1946, two articles were published from different groups in the 69th issue of Physical Review describing the phenomenon of nuclear magnetic resonance (NMR). Although the discovery of NMR by Purcell [1] and Bloch [2] was the beginning of an extensive development, it took nearly 30 years until this effect was used for the first time for imaging by Lauterbur [3]. Since then, magnetic resonance imaging (MRI) has progressed at a spectacular rate and started to become an important tool for clinical diagnosis with the first clinical trials in 1980.

Today, MRI is well-established in clinical routine, but still represents a continually evolving medical technology. With its excellent spatial resolution and its inherent high tissue contrast, MRI has surpassed computer assisted tomography for many clinical applications. However, this development did not occur overnight. Due to initial methodological constraints such as acquisition “dead times” imposed due to long $T_1$ relaxation times and technical constraints like radiofrequency (RF) and gradient hardware, main magnetic field strength, and field homogeneity, the first MRI methods required several minutes to nearly an hour to produce a two dimensional image of the human body with a resolution in the range of centimeters. The long scan times restricted the application of MRI as a diagnostic tool, increased the cost of scanning by limiting patient throughput, and led to image artifacts from patient motion during
scans. Early progress was in the improvement of signal-to-noise ratio (SNR) to reduce the need for signal averaging.

Since then, the evolution of MRI has been one of continued reduction in imaging time with numerous proposals to reduce the scan time. Besides advances in the technology of magnet construction, RF and gradient hardware, the development of fast imaging methods have drastically reduced scan times. With fast imaging sequences such as echo planar imaging (EPI) [4], fast low angle shot (FLASH) [5], turbo spin echo (TSE) [6] and fast imaging with steady precession (FISP) [7], complete MR images may be obtained hundreds to thousands of times faster than in the early years with comparable or even improved spatial resolution and contrast. Today, imaging times of a few seconds, yielding a resolution on the order of a millimeter, are common for clinical MRI. Based on these advances, new clinical applications have been developed, including real-time imaging of cardiac motion, multi-section imaging of the brain in a few seconds, and functional brain imaging (such as imaging of perfusion, diffusion and cortical activation). Fast imaging techniques have become the methods of choice for many applications, since they "freeze out" the effects of macroscopic motion, allowing a high scan efficiency and improved resolution.

Besides the image contrast, imaging speed is still probably the most important consideration in clinical MRI. Unfortunately, current MRI systems already operate at the limits of potential imaging speed, due to the technical and physiological problems associated with rapidly switched gradient systems. Recently, a quantum leap in speed has been provided through the advent of parallel MRI (pMRI) [8]-[22]. Instead of relying on increased gradient performance for increased imaging speed, pMRI extracts extra spatial information from an array of surface coils, resulting in an accelerated image acquisition. The acquisition speed of the current generation of pMRI scanners is
up to 2-4 times higher than traditional MR systems which rely solely on gradients for image encoding. Acquisitions have been increased by up to a factor of 8-16 at research sites using specialized hardware. These MRI scanners have provided the greatest gain in imaging speed since the development of fast MRI methods in the 1980s.

Over the past ten years, pMRI has improved with higher speed-up factors, automatic coil sensitivity calibration mechanisms, and improved reconstruction algorithms. Additionally, during this time, the MR scanners themselves have also improved. The more advanced MR scanners today are equipped with an increased number of independent receiver channels, improved RF coil geometries and higher field strengths. Even though these developments have greatly improved the image quality and the robustness of pMRI acquisitions, there are still problems in the use of pMRI in many clinical applications. The strongest constraint for the use of pMRI is SNR. Applications which are already at the limit of SNR are clearly not suitable for acceleration by pMRI. As a rule of thumb, the use of pMRI will reduce the attainable SNR by a factor of at least the square root of the acceleration factor. Besides the SNR issue, residual fold-over artifacts, originating from inaccurate pMRI reconstructions, are a second source of problems. There is a complicated relationship between the accuracy of a pMRI reconstruction and the imaging set up, which is not yet well understood. Since it is not possible to model this relationship and find a simple and robust solution for this problem, dedicated pMRI reconstructions are necessary for certain applications.

One possible solution to those problems is the synergy of a combination of more advanced sampling schemes such as non-Cartesian sampling strategies and pMRI. Although pMRI can benefit from the advantages of non-Cartesian trajectories and vice versa, the combination of these acquisition schemes with parallel imaging has yet not entered routine use. The main reason is the long
reconstruction time due to the complex calculations necessary for non-Cartesian parallel imaging.

This thesis is a summary of my developments and results on the research topic of fast non-Cartesian pMRI methods. The ideas presented in this work have led to new reconstruction algorithms enabling pMRI reconstruction times on the order of those for conventional Cartesian pMRI. The results of these advanced pMRI methods indicate the possibility to obtain higher acceleration factors or improved image quality compared to standard Cartesian pMRI.

In the first section of this thesis, the basic principles of MRI are introduced, i.e., the phenomenon of nuclear magnetic resonance, signal creation and spatial encoding of the signal using magnetic field gradients. Further, the $k$-space concept will be introduced and Cartesian and non-Cartesian $k$-space sampling strategies will be described briefly. A more specific description of those trajectories is given in the corresponding chapters about non-Cartesian pMRI.

Chapter 3 is intended to be introductory to parallel MRI; it begins with the basic features of parallel imaging using arrays of RF coils, followed by a brief history of the development in this field. In the next sub section of chapter 3, a detailed introduction to parallel MRI is given. The last sub section of chapter 3 is devoted to the Cartesian GRAPPA technique.

In chapter 4, the new concept of a fast one dimensional (1D) non-Cartesian GRAPPA method is introduced. It is shown that 1D non-Cartesian GRAPPA is more robust compared to Cartesian GRAPPA. Compared to previous non-Cartesian pMRI methods, the reconstruction time is in the range of the time required for Cartesian pMRI reconstructions.

Chapter 5 deals with a new concept of a direct spiral GRAPPA technique. This new method allows one to obtain significantly improved single shot spiral acquisitions compared to conventional spiral imaging. In this new method, the
reconstruction time is reduced to the same or even less than the time required for conventional data gridding.

Finally, the results and the significance of fast and direct pMRI methods with non-Cartesian sampling strategies are discussed.
# 2 Basic Principles of MRI

## 2.1 The Nuclear Magnetic Resonance Phenomenon

### 2.1.1 Nuclei in a Magnetic Field

Nuclear magnetic resonance (NMR) is the basic underlying phenomenon behind MRI. An object, e.g. a human being, is placed into a strong magnetic field. This field is typically in the range of 0.5 to 3.0 Tesla in clinical settings, which is ten to sixty thousand times the strength of the earth’s magnetic field. Such a strong magnetic field causes the nuclear spins of certain atoms within the body, namely those atoms that have a nuclear spin dipole moment, to orient themselves parallel or anti-parallel to the static main magnetic field ($B_0$). The nuclei spins precess about $B_0$ with a frequency, called the resonance or Larmor frequency ($\omega_0$), which is directly proportional to $B_0$:

$$\omega_0 = \gamma B_0$$  \hspace{1cm} (2.1)

where $\gamma$ is the gyromagnetic ratio, a fundamental physical constant for each nuclear species, which is listed for a few nuclei in Table 2.1. The Larmor relationship given by Equation 2.1 is the fundamental MR equation. Since the proton nucleus ($^1$H) has a high sensitivity (a result of its high gyromagnetic ratio, 42.58 MHz/Tesla) and a high natural abundance, it is currently the nucleus of choice for MRI. Due to the fact that the parallel state is the state of lower energy, slightly more spins reside in the parallel state than in the anti-parallel
state. This builds up a net magnetization $M_0$ which is oriented along the direction of the main field $B_0$.

<table>
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<th>Spin Quantum Number</th>
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<td>$^1$H</td>
<td>$\frac{1}{2}$</td>
<td>42.58</td>
</tr>
<tr>
<td>$^2$H</td>
<td>1</td>
<td>6.55</td>
</tr>
<tr>
<td>$^{13}$C</td>
<td>$\frac{1}{2}$</td>
<td>10.71</td>
</tr>
<tr>
<td>$^{19}$F</td>
<td>$\frac{1}{2}$</td>
<td>40.08</td>
</tr>
<tr>
<td>$^{23}$Na</td>
<td>$\frac{3}{2}$</td>
<td>11.26</td>
</tr>
<tr>
<td>$^{31}$P</td>
<td>$\frac{1}{2}$</td>
<td>17.25</td>
</tr>
</tbody>
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Table 2.1: Spin quantum numbers and gyromagnetic ratios for some atomic nuclei, which can be used for MRI.

### 2.1.2 Radiofrequency Field

A second magnetic field, termed the $B_1$ field, which oscillates at the Larmor frequency is applied using a RF coil. This RF pulse excites the nuclear spins and tips the net magnetization $M_0$ away from its equilibrium position. The net magnetization $M_0$ starts to precess around the axis of the static main field $B_0$ (longitudinal direction) at Larmor frequency $\omega_0$, which is shown schematically in Figure 2.1a. Due to the rotation of $M_0$ from the $z$ axis into the $xy$, or transverse plane, a transverse component $M_T$ of the vector $M_0$ is built up, while a longitudinal component $M_L$ remain along the $z$ axis. The transverse magnetization orthogonal to the longitudinal direction precesses at the Larmor frequency around the direction of the main field. During the application of the $B_1$ field the net magnetization rotates not only around the $z$ axis at Larmor frequency, but also moves away from the equilibrium state.
In the rotating frame system, which rotates at Larmor frequency around the $z$ axis, this motion of the net magnetization is simply a rotation from the longitudinal direction into the transverse plane. The amount of this rotation of the net magnetization $M_0$, away from its' equilibrium state is given in terms of the tip angle, which depends upon the duration and strength of the RF pulse.

2.1.3 MR Signal

The time dependent precession of the transverse magnetization induces a current in a receiver coil, the RF coil, according to Faraday’s Law of Induction. The resultant exponential decaying voltage, referred to as the free induction
decay (FID), constitutes the MR signal which can be described by the following equation:

\[
S(t) = \int \rho(\vec{r})e^{i\omega_0 t + \Phi} d^3r
\]  

(2.2)

where \(\rho(\vec{r})\) is the three dimensional spin density of e.g. protons inside the volume \(d^3r\).

### 2.1.4 Magnetic Field Gradients

By applying a linear magnetic field gradient along a single direction, the magnetic field strength is now directly related to the position along that direction. We have now created a spatially dependent magnetic field strength, which corresponds according to Equation 2.1 to a spatially dependent resonance or Larmor frequency, which can be used for spatial encoding of the MR signal.

### 2.2 Magnetic Resonance Imaging

#### 2.2.1 Slice-selective excitation

The first dimension is encoded by a so-called slice-selective excitation, which means that only spins from a well-defined slice of the object contribute to the MR signal. This is achieved by applying a magnetic field gradient along the \(z\) axis during an RF excitation pulse with a specific frequency bandwidth. When the slice-select gradient, \(G_{\text{Slice}}\), is applied along the \(z\) axis, the resonance frequencies of the protons become linearly related to the position along the \(z\) axis. Individual resonance frequencies correspond to individual planes of nuclei. In this example, these planes are oriented perpendicular to the \(z\) axis. When the
frequency-selective RF pulse is applied while $G_{\text{Slice}}$ is on, only nuclei in the plane with corresponding frequencies will be excited; thus a slice will be selected. The frequency bandwidth of the excitation pulse, together with the gradient, confines the excitation to the nuclei in the slice. No signals are excited from areas outside the defined slice.

### 2.2.2 Phase-encoding

After the slice-selective excitation, the next step is to encode the two dimensions within this slice. This is realized by imposing a spatially dependent phase on the signal from the precessing protons (phase-encoding) and by creating a spatially dependent frequency during signal reception (frequency-encoding). A spatially dependent phase can be created by applying a variable phase-encoding gradient, $G_{\text{Phase}}$, before the signal is received. If the direction of $G_{\text{Phase}}$ is denoted by $y$, during the phase-encoding period, nuclei along the $y$ direction experience different magnetic fields and therefore precess with different Larmor frequencies. After a certain period the phase-encoding gradient is turned off before data acquisition begins. After $G_{\text{Phase}}$ is turned off, all nuclei revert to the resonance frequency determined by the main magnetic field. The net effect of applying $G_{\text{Phase}}$ is to introduce a spatially dependent phase shift into the signal.

### 2.2.3 Frequency-encoding

The final spatial dimension, the $x$ direction, can be encoded into the signal by applying a gradient during the acquisition of the signal. The application of this gradient creates a spatially dependent Larmor frequency; therefore, this
gradient is referred to as the frequency-encoding gradient ($G_{\text{Freq}}$). Since the MR signal is sampled during the time that $G_{\text{Freq}}$ is on, this period is also commonly referred to as the read-out period and $G_{\text{Freq}}$ as the read gradient. A depiction of a basic MR sequence with slice-selective excitation, phase-encoding and frequency-encoding is shown in Figure 2.2. The conventional gradient-echo sequences are repeated at time intervals equal to TR, the so-called repetition time.

![Image](image_url)

**Figure 2.2:** Schematic depiction of a basic MR imaging sequence diagram using gradients for slice-selective excitation (together with the RF pulse), phase-encoding and frequency-encoding. The sequence shown here is repeated numerous times ($N_{\text{Phase}}$), each time with a different strength of the phase encoding gradient, which is indicated by an arrow. For each repetition $N_{\text{Freq}}$ data points are sampled, to finally build up an $N_{\text{Phase}} \times N_{\text{Freq}}$ data set.
The number of times the sequence is repeated (for one average) is determined by the desired spatial resolution, which is proportional to the number of voxels along the phase-encoding direction and is equal to the number of phase-encoding steps \( N_{\text{Phase}} \). For a certain number of averages \( N_{\text{AV}} \) the total time required to obtain an image slice is \( T_R \times N_{\text{Phase}} \times N_{\text{AV}} \). Typical parameters for a conventional spin-echo sequence are a \( T_R \) of 2000 ms and 256 phase encoding steps without averaging giving a total acquisition time of 8.5 min.

### 2.3 \( k \)-space concept

As shown in the previous chapter, the MR signal can be spatially encoded, after the slice-selective excitation, by applying magnetic field gradients in the remaining two dimensions. If it is assumed that the position of the magnetization with respect to the coils does not change with time (patient does not move), then the signal can be written as,

\[
S(t) = \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \rho(x, y) e^{i(\omega t + \Phi_x)} \, dx \, dy = \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \rho(x, y) e^{i\int_{0}^{T} G_x(t) \, dt + i\int_{0}^{T} G_y(t) \, dt} \, dx \, dy \tag{2.3}
\]

Making the following substitution,

\[
k_x = \gamma \int_{0}^{T} G_x(t) \, dt \quad \text{and} \quad k_y = \gamma \int_{0}^{T} G_y(t) \, dt \tag{2.4}
\]
then Equation 2.3 becomes

\[
S(k_x, k_y) = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \rho(x, y) e^{ik_x x + ik_y y} \, dx \, dy
\]  

(2.5)

This signal, in the so-called \( k \)-space, is the 2D Fourier transform of the spin density distribution, \( \rho(x, y) \), created by applying gradients in two dimensions. It represents the frequency spectrum of the spin density distribution of the underlying object. A measure of this spin density distribution, an image corresponding to the spatial variation in proton density, can be obtained by taking an inverse two dimensional Fourier transformation of the collected signals. The \( k \)-space concept was first described by Ljunggren [23].

### 2.4 \( k \)-space sampling

#### 2.4.1 Cartesian trajectories

In general, the whole of \( k \)-space data is not sampled after a single excitation. There are physical limitations such as a finite relaxation time and the SNR and there are technical limitations such as the slew rate of the gradients. Thus \( k \)-space is sampled in a sequential way by repeating a sequence \( N_{\text{Phase}} \) times. During each repetition a signal is sampled along a line in \( k \)-space corresponding to a certain position \( nk_y \) in \( k \)-space, which is depicted in Figure 2.3. This \( k \)-space sampling method is referred to as 2D Fourier or spin-warp imaging [24].

There are some important relationships between the sampled data in \( k \)-space and the corresponding image in the image domain.
The distance between two adjacent data points in $k$-space dictates the FOV of the image. A larger step size in $k$-space corresponds to a smaller FOV and vice versa.

\[
\Delta k_x = \frac{2\pi}{\text{FOV}_x} \\
\Delta k_y = \frac{2\pi}{\text{FOV}_y}
\]  

(2.6)
Further, the $k$-space extent which is covered by the sampled data defines the resolution in the image and is given by:

$$\Delta x = \frac{2\pi}{N_{\text{Freq}} \Delta k_x}$$

$$\Delta y = \frac{2\pi}{N_{\text{Phase}} \Delta k_y}$$  \hspace{1cm} (2.7)

One of the most important advantages of Fourier imaging is that the reconstruction can be performed with a simple and fast inverse Fourier transformation. A requirement of the Fourier transformation is that the $k$-space data are obtained on a rectangular grid with equidistant step size in each of the directions. Those sampling schemes with constant distance between measured data points in each direction are named Cartesian trajectories.

### 2.4.2 Non-Cartesian trajectories

Compared to 2D Fourier imaging with Cartesian trajectories, data acquired on non-Cartesian trajectories are not aligned on a rectangular grid with equidistant sampling density. For those sampling schemes, first described by Twieg [25],[26], reconstruction has to be performed with methods different than the Fourier transformation.

Non-Cartesian sampling can be performed in one direction, while the remaining direction is sampled with constant distance. This sampling strategy is named one dimensional (1D) non-Cartesian sampling (see Figure 2.4a).
There are numerous two dimensional (2D) non-Cartesian trajectories. In Figure 2.4 two common 2D non-Cartesian trajectories are depicted. A radial sampling scheme is shown in Figure 2.4b and a spiral trajectory is shown in Figure 2.4c.

Both trajectories enable fast dynamic acquisition methods especially used e.g. for cardiac cine imaging or functional MRI. A detailed description of the 1D non-Cartesian trajectory will be given in chapter 4.2.2, while the spiral trajectory is described in detail in chapter 5.2.1
3 Basic Principles of Parallel MRI

3.1 Introduction

The basic idea how the data acquisition can be accelerated with parallel imaging in MRI, is rather simple. The acquisition time is directly dependent on the amount of data to be acquired for an MR image. By reducing the amount of image data needed to create the image, the acquisition time is also reduced. The idea of reducing the amount of \( k \)-space data is not new; as a rule, the resolution, and therefore the extent of \( k \)-space, is tailored specifically to the type of diagnostic analysis being performed. In Figure 3.1, this idea is explained schematically. It is assumed that \( k \)-space is acquired in a sequential way line-by-line, which is the case in most MR sequences used for clinical exams. As explained in chapter 2.4.1, the distance between neighboring \( k \)-space lines is determined by the desired FOV in the image domain. A larger FOV corresponds to a smaller separation between \( k \)-space points. In order to make a high-resolution image with a specific FOV (Figure 3.1a), the extent of \( k \)-space acquired must be greater than for a low-resolution image with the same FOV (Figure 3.1b). An image with a lower resolution shows not only blurring but also other image artifacts, most noticeably Gibbs ringing.

A common method for shortening the image acquisition time without reducing the resolution is the use of half-Fourier procedures [27],[28].
As shown in Figure 3.1c, only one half of the $k$-space data is acquired in this method. The corresponding image obtained without a half-Fourier reconstruction is noticeably worse than the reference image made using the entire $k$-space, as less frequency-differentiating data has been acquired. In practice, a few $k$-space lines in the other half of $k$-space are also acquired. These extra lines allow a half-Fourier reconstruction of the missing portion of $k$-space through the use of appropriate algorithms. In this procedure, a maximal
“acceleration factor” of two is possible, as the acquisition of less than half of the k-space data makes the reconstruction of missing data points impossible.

Unlike in half-Fourier imaging, parallel imaging or parallel MRI (pMRI), functions by reducing the k-space data by increasing the distance between neighboring lines. The FOV in the image domain is thus reduced, leading to fold-over artifacts, otherwise known as aliasing, when the object to be imaged is larger than the decreased FOV. As an example, Figure 3.1d shows a k-space reduced by a factor of two, where every second line has been left out. Such an acquisition scheme is known as “reduced k-space,” where the reduction factor, which is also known in pMRI as the acceleration factor (AF), is denoted by the letter $R$. By using a reduced sampling with $R=2$, the FOV in the image domain is reduced by half, and it is possible that the original image no longer fits into the smaller FOV. A simulation of such a case is shown in Figure 3.1d. All portions of the object outside of the FOV are folded back into the FOV because the Nyquist criterion has not been fulfilled for the complete image. In comparison with the reference image in Figure 3.1a, the acquisition time for such a folded image is reduced by a factor of two in comparison to a fully-acquired image, but it is obvious that images with these severe aliasing artifacts are not usable in clinical diagnosis. In general, parallel imaging works by removing aliasing artifacts through the reconstruction of the missing k-space lines or by “unfolding” the folded image. To this effect, parallel imaging necessitates the use of several independent coils and a corresponding number of receiver channels on the MR system. In order to employ the coil set-up as spatial information for the pMRI reconstruction, the k-space data from each coil must be simultaneously and independently acquired. One can imagine a simplified set-up, which is depicted in Figure 3.2, where each coil receives signal only from a limited portion of the object.
Figure 3.2: Schematic depiction of a simplified parallel imaging procedure. (a) Full acquisition using a volume coil, $N_{\text{Phase}}$ phase encoding steps are required. (b) Two surface coils, each with a boxcar-like sensitivity profile over the FOV in phase encoding direction. (c) Full acquisitions with these surface coils. The range of sensitivity covers approximately half of the FOV. (d) Half FOV acquisition with $N_{\text{Phase}}/2$ phase encoding steps. (e) Combination of the two images to obtain a full FOV image. This figure is reprinted from reference [71].
The acquisition covers a reduced FOV in the image domain, and thus a reduced $k$-space, but does so simultaneously for several receiver coils which acquire information from different spatial locations in the object separately.

If the individual coil images are examined together, an image of the complete object can be obtained. This method of arriving at a complete image using the reduced $k$-space data from multiple coils is the simplest form of pMRI, and is known as PILS [22]. This straightforward technique only works for coils with localized sensitivities, thus in most cases, only small coils. For the coils normally used in clinical MR scanners, more advanced techniques which take the variations in coil sensitivity into account more accurately than PILS must be used.

3.2 A Short History of Parallel MRI

In parallel imaging the number of phase-encoding steps and therefore the acquisition time is reduced compared to conventional imaging. Due to the parallel imaging reconstruction procedure the same field of view with the same spatial resolution as in conventional MRI can be obtained even with reduced phase-encoding steps. This is possible, because multiple independent receiver coils are used, and the spatial information content of the coils in the array is exploited to encode and detect multiple MR echoes simultaneously. The key element of any pMRI system is the application of multiple independent receiver coils with distinct sensitivities across the object. Traditionally, the main purpose of this so called phased array technology [29],[30] was to distribute the high SNR performance of their small component coils over a larger area covered by the entire array, with no increase in imaging time. Whereas in conventional
imaging phased array technology has been used to improve image quality within the same acquisition time, pMRI techniques are using phased array technology to provide a significant reduction of MR scan time.

In 1988, before the introduction of the phased array technology in MRI, an early theoretical proposal for a massively parallel imaging strategy was made [8]. The phase-encoding gradient steps were entirely replaced by the use of multiple detectors. In this approach the number of coils in the underlying coil array approached the number of $k$-space lines to be acquired for an image. A subsequent proposal [9],[10] for massively parallel imaging included a more detailed investigation of feasibility issues, although no image data were presented.

In current pMRI techniques, the number of coils is significantly smaller than in the early massively parallel approaches, and therefore technically feasible and much cheaper. The aim of the pMRI approach is to partially replace the time consuming gradient encoding steps for image formation. An early proposal for pMRI using a coil array was made in 1989 [11]. A similar approach was subsequently described [12], and the first phantom images demonstrating the underlying principle were presented. This pMRI principle, dubbed subencoding, involves an “unaliasing” of reduced FOV images. This is achieved by applying the knowledge of individual coil sensitivity functions in combination with a pixel-by-pixel matrix inversion to the (reduced FOV) component coil images. This “unaliasing”-procedure is performed in image space. An optimized and more general approach of subencoding named SENSE (sensitivity encoding) [13] was presented in 1999.

The first description of a pMRI technique performed in $k$-space was presented in 1987 [14], and a further approach, where missing $k$-space lines were generated from a series expansion of reduced $k$-space raw data sets in two coils with distinct sensitivities (one homogeneous volume coil and one coil with
a constant sensitivity gradient), was presented in 1993 [15]. Even though these methods never fully worked, they paved the way for the first successful in vivo pMRI implementation, the Siemens Multaneous Acquisition of Spatial Harmonics (SMASH) [16]. Since the introduction of SMASH in 1997 many new approaches have been proposed to perform in vivo parallel imaging in $k$-space with greater robustness and with less effort. One year later, in 1998 the first self-calibrating technique named AUTO-SMASH [17] was introduced. This method avoids the necessity of coil sensitivity estimation and therefore works completely in $k$-space. These regenerative $k$-space pMRI techniques, namely SMASH and AUTO-SMASH, were further developed and improved [18]-[20].

Besides the regenerative $k$-space and the image domain based pMRI techniques, a third group of so named hybrid techniques, the method Sensitivity Profiles from an Array of Coils for Encoding and Reconstruction In Parallel (SPACE RIP), was introduced in 2000 [21]. To summarize, all modern parallel imaging methods can be classified into three groups, namely image domain based techniques (SENSE, PILS), hybrid techniques (SPACE RIP) and regenerative $k$-space methods (SMASH, AUTO-SMASH, GRAPPA). In this classification, the self-calibrating techniques play a special role, because these techniques do not rely upon accurate knowledge of coil sensitivities.

### 3.3 k-Space Based Parallel MRI

In order to understand the Cartesian and the non-Cartesian GRAPPA methods, we first summarize the basic concepts of the $k$-space based pMRI techniques SMASH, AUTO-SMASH and VD-AUTO-SMASH.
In the original SM ASH manuscript [16], it was shown that it is possible to reconstruct many lines of \(k\)-space from a single acquired line. SMASH achieves this encoding efficiency in that it uses combinations of signals from an array of surface coils to mimic directly the spatial-encoding normally performed by phase-encoding gradients. In this approach signals from the various array components are combined by appropriate linear combinations of component coil signal with different complex weights \(n_i^{(m)}\), to generate composite coil sensitivity profiles \(C_{m}^{\text{Comp}}\) with sinusoidal spatial sensitivity variations (spatial harmonics of order \(m\)) on top of the original coil sensitivity profile \(C_{0}^{\text{Comp}}\):

\[
C_{m}^{\text{Comp}}(x, y) = \sum_{l=1}^{L} n_i^{(m)} C_l(x, y) = C_{0}^{\text{Comp}} \exp\{ im\Delta k_y y \}
\] (3.1)

Here \(C_l\) is the coil sensitivity function of coil \(l\) at position \((x, y)\), where \(l\) counts from one to \(L\) for an array coil with \(L\) elements and \(m\) is an integer which specifies the spatial harmonic number. If the composite sensitivity profiles generated in this way match the spatial harmonic modulations of the phase-encoding gradients, the resulting signal of such a combination is a \(k\)-space signal shifted by precisely the same amount \((m\Delta k_y)\) as would have resulted from a traditional gradient step:

\[
S_{m}^{\text{Comp}}(k_x, k_y) = \iint dx dy C_{m}^{\text{Comp}} \rho(x, y) \exp\{ ik_x x + ik_y y \} =
\]

\[
= \iint dx dy C_{0}^{\text{Comp}} \rho(x, y) \exp\{ ik_x x + i( k_y + m\Delta k_y) y \}
\] (3.2)

For accurate reconstruction, the SMASH technique relies upon accurate knowledge or estimation of the relative RF coil sensitivities of the component coils in the array in order to determine the optimal complex weights \(n_i^{(m)}\).
Therefore, the most important step in a practical SMASH implementation is to measure the sensitivities of the various array elements. This is a non-trivial problem in vivo, since many factors affect the NMR signal besides coil sensitivity variations, making extraction of coil sensitivity information difficult. There may be additional effects of coil loading that are subject dependent which can not be easily modeled and may result in unpredictable behavior. In general, in vivo coil sensitivity calibration can be a problematic, inaccurate and also time consuming procedure in many cases, especially in the situation of low SNR and tissue motion. This problem occurs in all pMRI methods based on either the SMASH or the SENSE approaches.

The AUTO-SMASH approach avoids these limitations by recording a small number of additional auto-calibration signals (ACS) during the actual scan, which serve as target lines for a fit procedure. The ACS-lines are added to the

\[
\Delta k_y = \frac{2\pi}{FOV}
\]

Figure 3.3: k-space sampling scheme for AUTO-SMASH. Measured k-space lines (source lines) are indicated by solid lines, missing k-space lines are indicated as dotted (small dots) lines, the additional measured ACS-lines (target lines) at intermediate position are indicated as dotted (big dots) lines. (a) For a reduction factor \( R=2 \), only every second line plus one single ACS-line is measured. (b) and (c) show the sampling scheme for reduction factors \( R=3 \) and \( R=4 \). This figure is reprinted from Reference [18].
acquisition, which is shown schematically in Figure 3.3 for reduction factors from 2-4 (Figure 3.3a - Figure 3.3c).

In general, if $R$ stands for the reduction factor, $(R-1)$ extra navigator ACS-lines are acquired, which are exactly shifted by an amount of $m\Delta k_y$ ($m=1,...,R-1$).

Thus the ACS navigator signals represent lines at intermediate positions in $k$-space, which are phase-encoded in a conventional manner using the phase-encoding gradient. The relation between these target lines $S_i^{ACS}$ and the usual measured source lines $S_i$ are then used to "train" the AUTO-SMASH reconstruction directly in $k$-space. The set of complex weights $n_i^{(m)}$ can be determined automatically without the intermediate step of coil sensitivity.

\[
S_{ACS}^{l} (k_y + m\Delta k_y) \cdot n_l^{(0)} = S_{Comp} (k_y + m\Delta k_y)
\]

Figure 3.4: Determination of the coil-weights for a four-element array coil. Here, measured source lines $S_i(k_y)$ are fitted to the target, a single composite ACS-line $S_{Comp}^{l}(k_y + m\Delta k_y)$, which is shifted by $m\Delta k_y$, yielding the desired coil-weights. This figure is reprinted from Reference [18].
measurements, by using the relations between the conventional acquired data set and the extra acquired ACS-data. A schematic depiction of this procedure is shown in Figure 3.4 for a four-element array.

The desired optimal complex weights \( n^{(m)}_i \) are determined from the following fit function:

\[
S_{\text{Comp}}(k_y + m\Delta k_y) = \sum_{l=1}^{L} n^{(m)}_l S_l(k_y) = \sum_{l=1}^{L} n^{(0)}_l S^{dCS}_l (k_y + m\Delta k_y)
\]  

(3.3)

In Equation 3.3, \( S_{\text{Comp}} \) stands for the target line, the composite ACS-line which is shifted precisely \( m\Delta k_y \) from the conventional signal \( S_l(k_y) \). This expression can be written in matrix form, which leads to the following equation for a four-element coil array:

\[
\begin{pmatrix}
S_{\text{Comp}}(k_1, \ldots, k_N, k_y) \\
S_{\text{Comp}}(k_2, \ldots, k_N, k_y) \\
S_{\text{Comp}}(k_3, \ldots, k_N, k_y) \\
S_{\text{Comp}}(k_4, \ldots, k_N, k_y)
\end{pmatrix}
= \begin{pmatrix}
n^{(m)}_1 \\
n^{(m)}_2 \\
n^{(m)}_3 \\
n^{(m)}_4
\end{pmatrix}
\begin{pmatrix}
S_1(k_1, \ldots, k_N, k_y) \\
S_2(k_1, \ldots, k_N, k_y) \\
S_3(k_1, \ldots, k_N, k_y) \\
S_4(k_1, \ldots, k_N, k_y)
\end{pmatrix}
\]  

(3.4)

\( S_{\text{Comp}} \) and \( S_l \) now indicate vectors with \( N_x \)-elements, where \( N_x \) is the number of sampled data points in the read-direction. The determination of the unknown coil-weights from this over-determined linear equation system is a so-called inverse problem. The solution of this inverse problem can be obtained, for example using the Moore-Penrose pseudo-inverse:

\[
n^{(m)}_l = S_{\text{Comp}} S^*_l (S_l S^*_l)^{-1}
\]  

(3.5)
In Equation 3.5, $\mathbf{n}_l^{(m)}$ stands for the vector of the $l$ complex coil-weights, $S_{\text{Comp}}^l$ is the vector of the target-line, composite auto-calibration signal and $S_{l}^\dagger$ is the transposed complex conjugate matrix of the $l$-source lines. Implementation of the problem in this way also facilitates the incorporation of numerical conditioning into the process.

In summary, the AUTO-SMASH self-calibration procedure replaces an experimentally cumbersome and potentially inaccurate coil sensitivity measurement with a targeted acquisition of a few extra lines of NMR signal data. Acquisition of the extra ($R-I$) navigator lines adds only a very small amount to the total acquisition time, and allows direct "sensitivity calibration" for each image, even in regions of inhomogeneous spin density and regardless of coil loading. If flexible coil arrays are used, AUTO-SMASH can provide accurate calibrations even if array positions change from scan to scan.

Further improvements of the AUTO-SMASH technique were achieved by using a variable density acquisition scheme, which is based on the assumption that some parts of $k$-space can be measured with more accuracy than others. In most imaging situations, the signal energy content of $k$-space lines decreases with increasing phase-encoding values. This is the essential basis for many imaging concepts and also the essential basis for the variable density (VD-) AUTO-SMASH approach [18]. VD-AUTO-SMASH is in spirit similar to the work presented by Luk et al. [31], who addresses flow artifacts in echo-planar imaging, Weiger et al. [32], who addresses respiratory motion artifacts and Chi-Ming Tsai [33] who addresses aliasing artifacts using a variable density $k$-space sampling trajectory. Since AUTO-SMASH is a pure $k$-space related PPA technique, it is well suited to variable density sampling. In this approach we reduce residual aliasing artifacts by exploiting the property that in most images the energy is concentrated around the $k$-space origin.
If \( k\)-space is uniformly undersampled, then aliasing artifacts will be dominated by low-frequency components. These low-frequency, high-energy artifacts can be avoided in imperfect AUTO-SMASH reconstruction by sampling the central \( k\)-space with a density corresponding to a standard full FOV acquisition. The sampling density above a certain cutoff-spatial frequency (COSF) is then decreased to a "standard" reduced density, \( 1/R \). In the outer parts of \( k\)-space above the COSF the reduction factor is \( R \), which we now refer to as

\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{k-space_sampling.png}
\caption{Different \( k\)-space sampling schemes. (a) Fully sampled acquisition used for the reference scan. (b) Reduced AUTO-SMASH acquisition with acceleration factor of 2 (only one ACS-line) and (c) a VD-AUTO-SMASH acquisition with 3 additional ACS-lines and outer reduction factor of 4. On the bottom row, the corresponding density functions are plotted schematically. This figure is reprinted from Reference [18].}
\end{figure}
outer-reduction factor (ORF). The new $k$-space sampling pattern for VD-AUTO-SMASH is shown schematically in Figure 3.5c.

For comparison, the $k$-space sampling scheme of a full time reference acquisition and the conventional AUTO-SMASH acquisition are shown in Figure 3.5a and Figure 3.5b. In the same figure the corresponding sampling density functions are also plotted on the bottom row.

In VD-AUTO-SMASH several ACS-lines for each harmonic are acquired in the center of $k$-space. These extra acquired lines reduce the high-energy fold-over artifacts when they are included in the final image reconstruction, while at the same time they also allow an improved determination of the coil-weights. In general, the improvement with this variable density approach comes at the expense of a longer scan time, which adds $(R - 1 + N_{extra}) \times T_R$ to the accelerated scan time, where $N_{extra}$ stands for the number of additional acquired ACS-lines in the center of $k$-space and where $T_R$ represents the repetition time of the applied imaging technique.

One important practical aspect of the VD-AUTO-SMASH acquisition is the possibility of improved fitting, achieving a reduction in the variability of the coil-weighting factor estimation. In the following we present an algorithm which allows one to extract improved values of the coil-weighting factors from noise-corrupted ACS observations. In the original AUTO-SMASH approach, only one fit between two individual lines was used to determine the coil-weights for the corresponding shift in $k$-space. In the VD-approach, the acquisition of extra ACS-lines provides the possibility to improve this fit by taking advantage of several additional fitting combinations. This is shown schematically in Figure 3.6b for a VD-AUTO-SMASH acquisition with $ORF = 4$ and 6 ACS-lines in total. In the original AUTO-SMASH approach, just one fitting combination would be used to determine the first coil-weights (see Figure 3.6a). The more
sophisticated VD-AUTO-SMASH scheme shown in Figure 3.6b enables seven additional fits (eight in total).

\[ \Delta k_y = \frac{2\pi}{\text{FOV}} \]

**Figure 3.6:** AUTO-SMASH (a) versus VD-AUTO-SMASH (b) acquisition scheme. (a) In AUTO-SMASH only the fit between one source line and the corresponding ACS-line is used to determine the coil-weights. (b) The improved scheme of the VD-approach enables 7 additional fits. (c) Graphical depiction of how to combine the signals, to generate the enlarged matrix of the coil data sets (bright gray block) and the enlarged vector of the composite signals (dark gray block). This figure is reprinted from Reference [18].
One straightforward approach would be to simply average these 8 sets of fitted coil-weights. The main drawback of this approach is, however, that the estimation of coil-weights with ACS-lines from the outer part of \( k \)-space, with significantly reduced SNR, is strongly affected by noise, see [17].

A \textit{weighted averaging} scheme takes the signal energy content of each particular \( k \)-space line into account. It is depicted in Figure 3.6b. The two regular measured source lines \( S_i(k_y + m \Delta k_y) \) (with \( m = 0,4 \)) and the 6 ACS-lines \( S_i(k_y + m \Delta k_y) \) (with \( m = 1,2,3,5,6,7 \)) are composed in a way such that these 8 coil data sets built an \( 8 \cdot N_x \times N_{\text{Coil}} \) coil data matrix, where \( N_x \) is the number of sampled points in read-direction and \( N_{\text{Coil}} \) is the number of coils in the array. This is shown schematically in Figure 3.6c, where the data sets of the above described lines, which are indicated by the bright gray block, are stacked into a matrix. The vector of the composite signals is constructed in the same manner, but every line is shifted by \( \Delta k_y \) (indicated by the dark gray block in Figure 3.6c).

The estimation of the coil-weights is then performed with a fit between the enlarged matrix and the enlarged vector. In this example, the matrix and the vector are eight times larger compared to those vectors shown in Figure 3.4. In Figure 3.6 only the estimation of the coil-weights, \( n_i^{(1)} \), for a shift about \( \Delta k_y \) is indicated.

However, it is straightforward to apply the same procedure for larger shifts in \( k \)-space. By computing the Moore-Penrose pseudoinverse in this way, the relative contribution of the different lines are weighted by the square of their intensity, which is equivalent to the energy of the respective \( k \)-space lines.
3.4 Cartesian GRAPPA

A more generalized implementation of the VD-AUTO-SMASH approach [18] is the GeneRalized Autocalibrating Partially Parallel Acquisitions (GRAPPA) method. The major difference in GRAPPA is the possibility to reconstruct uncombined coil images for each coil in the array. Further, compared to VD-AUTO-SMASH, more data are incorporated into the fit procedure, which improves the accuracy of the fit procedure. This process is shown schematically in Figure 3.7. Here, data from measured target lines in each individual coil of the array (solid black lines) are used to fit data of a single source line (solid blue line) of a single coil. This fit gives the weights which can then be used to generate the missing lines from that coil. Once all of the lines are reconstructed for a particular coil, a Fourier transform can be used to generate the uncombined image for that coil. This process is repeated for each coil in the array, resulting in four uncombined single coil images which can then be combined using a conventional sum of squares reconstruction [29].

In general, the process of reconstructing data in a specific coil $j$ at a line $(k_y, m\Delta k_y)$ offset from a normally acquired data line using a block wise reconstruction can be represented by:

$$S_j(k_x, k_y + m\Delta k_y) = \sum_{l=1}^{N_b} \sum_{m=0}^{N_b-1} n(j, l, m, b) S_l(k_x, k_y + b\Delta k_y)$$

(3.6)

where $AF$ represents the acceleration factor. $N_b$ is the number of blocks used in the reconstruction, where a block is defined as a single acquired line and $A-1$
missing lines. In Figure 3.7 this process is shown schematically for four coils and four blocks for each coil. In this case, \( n(j,l,m,b) \) represents the weights used in this now expanded linear combination. In this linear combination, the index \( l \) counts through the individual coils, while the index \( b \) counts through the individual reconstruction blocks.

**Figure 3.7:** Depiction of a Cartesian GRAPPA reconstruction: Data from measured target lines (solid black lines), from all coils (here coil #1 to coil #4) are used to reconstruct data from a single source line (solid blue line) of a single coil (here coil #3).
The GRAPPA reconstruction described in Equation 3.6 is formulated as a discrete shift. However, Equation 3.6 can be reformulated as a convolution on the $k$-space data [52]:

$$S_j(k_x, k_y + m\Delta k_y) = \sum_{l=1}^{L} \sum_{\tau_x, \tau_y} n^j(\tau_x, \tau_y) S_j(\tau_x - k_x, \tau_y - k_y)$$ (3.7)

In this more general description, the coil weights are represented by a two dimensional convolution kernel. A more detailed description of the choice of the GRAPPA kernel size and the influence on the final reconstruction will be given in the corresponding chapters about non-Cartesian GRAPPA.
4 **A Fast Method for 1D Non-Cartesian Parallel MRI**

4.1 **Introduction**

It has been shown, e.g. in [33]-[35], that non-Cartesian sampling trajectories can offer inherent advantages for MRI compared to Cartesian acquisition schemes. Spiral trajectories, for example, make optimal use of the gradient performance of an MR system, while radial sampling schemes are known to be very robust even in the case of vast undersampling. Radial and spiral trajectories are two-dimensional (2D) non-Cartesian sampling strategies. However, the use of trajectories which are non-Cartesian along one dimension in $k$-space and Cartesian along the other can also be advantageous. These so-called one-dimensional (1D) non-Cartesian trajectories can be designed and optimized for a robust fold-over artifact behavior. Even though the advantages of non-Cartesian trajectories are well-known, these trajectories are not in common use in clinical MRI. In comparison, it is standard in clinical routine to use parallel imaging [13],[19] to speed up the acquisition of MR examinations. However, parallel MRI (pMRI) is not without its limitations. All pMRI acquisitions are affected by an inherent SNR loss, which is, as a rule of thumb, at least proportional to the square root of the acceleration factor. Additionally, noise introduced by imperfections in the coil geometry and reconstruction algorithms further degrades the SNR. In the SENSE method [13], reconstruction is
performed in the image domain on a pixel-by-pixel basis. Therefore, errors in this procedure are local and appear as a kind of noise enhancement in the image. In comparison, the GRAPPA reconstruction [19] is performed in k-space using a fit procedure between adjacent k-space lines or data points. Since a single data line or data point in k-space affects the whole image in the image domain, errors in this procedure are global and appear as remaining fold-over artifacts in the final image. Therefore, the more relaxed fold-over artifact behavior of non-Cartesian trajectories is beneficial for such pMRI reconstructions. Non-Cartesian trajectories have another advantage for pMRI. Whenever they are designed to oversample a certain part or several parts of k-space, they are inherently autocalibrated. The autocalibration approach [17] is a method in which a few k-space data lines or points are sampled densely enough to fulfill the Nyquist criterion (and may be sampled so densely that they surpass the Nyquist criterion). The densely-sampled k-space data, otherwise known as the autocalibration signal (ACS), are then used to derive the reconstruction parameters, i.e. the coil weights. The ACS data can be acquired before, after, or during the actual accelerated scan. The acquisition of the ACS data during the accelerated scan as suggested in [18], the so-called variable density (VD) approach, has the advantage that the ACS data can be incorporated into the reconstructed data set. This can significantly increase the overall image quality of the reconstruction. From the VD approach in [18], where two different sampling densities were mainly used, it is a logical step to move to a continuously variable density sampling scheme using a 1D non-Cartesian trajectory. The more relaxed fold-over artifact behavior of non-Cartesian imaging makes such a trajectory an ideal complement to pMRI. Although parallel imaging can benefit from the advantages of non-Cartesian trajectories described above, and vice versa, the combination of these acquisition schemes with parallel imaging has yet not entered routine use. The main reason for that are
the long reconstruction times due to the complex calculations necessary for non-Cartesian parallel imaging.

In this chapter, which is based on the ideas presented at the 11th ISMRM Meeting in Toronto [36] and at the 20th ESMRMB Meeting in Rotterdam [37] in 2003, it is shown that one can greatly reduce complexity of the reconstruction procedure of 1D non-Cartesian pMRI, which is directly related to the reconstruction times. This is achieved by exploiting a specific property of the reconstruction parameters used for parallel imaging in $k$-space. The method presented here is a promising approach to overcome computational limits, which are still a hindrance for the use of non-Cartesian pMRI in clinical routine.

### 4.2 Theory and Methods

#### 4.2.1 Cartesian trajectories and pMRI

Even though discrete data points are sampled, it is common to depict the $k$-space coverage as a line by line acquisition as shown on the left side of Figure 4.1. Neglecting the dwell time, the Cartesian trajectory can be described by a one-dimensional function in $k$-space with a constant slope (dashed line on the right side of Figure 4.1). The distance between two adjacent sampling points along such a linear function is constant. This equidistant sampling corresponds to a constant sampling density in $k$-space, which is related to a certain FOV. In parallel imaging, the distance between measured adjacent data lines in $k$-space, the slope of the function, is increased by periodically skipping some fraction of the lines to be measured. Directly related to that is the acquisition speed or the acceleration factor ($AF$), when the resolution, the $k$-space coverage, is preserved. For example, measuring only every second line would result in an $AF$ of two. On the other hand, due to the increased sampling distance in $k$-space
the FOV is reduced by a factor of two, leading to aliasing when the object to be imaged is bigger than the reduced FOV. In a pure $k$-space based pMRI technique such as GRAPPA, missing $k$-space lines are reconstructed. This is accomplished by applying reconstruction parameters, the coil weights, to the measured $k$-space data to derive weighted linear combinations of those data. This process can be described as a convolution of the measured data with a two dimensional GRAPPA convolution kernel \cite{52}, i.e. a specific set of coil weights, to derive the missing data. In general, the coil weights exploit the spatial information of a coil array which is used for acquisition. The coil weights are calculated from the ACS data set using a fit procedure. In GRAPPA the full $k$-space is regenerated for each individual coil element.

\begin{figure}[h]
\centering
\includegraphics[width=\textwidth]{cartesian_non_cartesian_k_space.png}
\caption{Schematic depiction of the Cartesian and non-Cartesian $k$-space and the corresponding 1D trajectory plot: (left) The echoes in the Cartesian $k$-space (dashed lines) are sampled equidistantly, while the distance between sampled echoes in the non-Cartesian $k$-space (solid lines) varies. (right) The 1D trajectory plot runs from 1 to 256, covering a range between -128 $\Delta ky$ and 127 $\Delta ky$. The Cartesian trajectory plot (dashed) is a straight line with a certain slope, which is constant everywhere. Compared to that, the non-Cartesian trajectory plot (solid) is a curve with varying slope. The slope of the trajectory plot corresponds to the local $AF$. The Cartesian and the non-Cartesian trajectories cover the same $k$-space range; the starting and end points of both trajectories are identical. This figure is reprinted from Reference \cite{38}.}
\end{figure}
4.2.2 1D non-Cartesian trajectories

In comparison to the above, 1D non-Cartesian trajectories can be described as functions with a variable sampling density. Since the distance between measured data lines is no longer constant, a local acceleration factor \((LAF)\) must now be defined as the slope of the function at a specific position. As depicted on the right side of Figure 4.1, the Cartesian and the non-Cartesian trajectory cover the same \(k\)-space range (from -128 to +127) with the same number of echoes or \(k\)-space lines (from 1 to 256.) The non-Cartesian trajectories used for this study were designed to fulfill the following requirements:

1. The central part of the trajectory is a linear function, which is sampled at least at the Nyquist rate (or even more densely).

2. The sampling density of the outer parts of the trajectory decreases continuously.

3. The \(k\)-space position of the outermost point of the non-linear function is determined by the resolution, i.e. the desired \(k\)-space range.

4. The slope of this function at that specific point, or in other words, the distance between the two outermost points, which is the maximum local acceleration factor \((LAF_{Max})\), should not exceed a certain value.

5. The linear and the non-linear function should fit together smoothly (i.e. no discontinuities in the trajectory).
Since the trajectory itself is point wise symmetric around zero, only the functions describing the positive part of the trajectory are discussed. Assuming that the $k$-space step size $\Delta k_y$ corresponds to a Nyquist sampling rate, $\Delta k_y$ is normalized to one and the trajectory is defined by the following two basic functions:

\[
f_{\text{Linear}}(n) = \frac{n}{SD} = \frac{n}{OS \cdot AF} \quad n = [0, n_{\text{Linear}}] \text{ and } OS \geq 1 \quad (4.1)
\]

\[
f_{\text{Cubic}}(n) = An^3 + Bn^2 + Cn + D \quad n = [0, n_{\text{Cubic}}] \quad (4.2)
\]

Here, the parameter $n$ is an integer counter of the echoes or $k$-space lines which belong to the linear or to the non-linear part of the trajectory. $SD$ is the sampling density of the linear trajectory. $AF$ is the desired overall acceleration factor which is controlled by the choice of the FOV in the phase-encoding direction, and $OS$ is the oversampling factor of the central linear trajectory. To ensure that the linear trajectory is always oversampled, or sampled at least according to the Nyquist criterion, even in the case of an overall accelerated acquisition, $AF$ has to be taken into account in Equation 4.1. For the non-linear trajectory, a cubic function was chosen, because this type of function offers sufficient degrees of freedom to adapt this function to the requirements described above. The linear function in Equation 4.1 has a constant sampling distance between points along this trajectory. In comparison, the sampling distance of the non-linear function in Equation 4.2 has a sampling distance which depends upon the echo number ($n$). The sampling distance or the local acceleration factor can be defined as the slope of the function at a specific position.
To meet the requirements defined above, the following set of equations can be defined using Equation 4.1 – Equation 4.4:

\[ f'_{\text{Linear}}(n) = \frac{1}{OS \cdot AF} \quad OS \geq 1 \quad (4.3) \]

\[ f'_{\text{Cubic}}(n) = LAF(n) = 3An^2 + 2Bn + C \quad n = \left[0, n_{\text{Linear}}\right] \quad (4.4) \]
The properties of these expressions are depicted in Figure 4.2. A linear reference function (thin straight line in Figure 4.2) covers a $k$-space range of $n_{\text{Ref}} \cdot \Delta k_y$, where $n_{\text{Ref}}$ is the number of echoes of the positive reference trajectory without undersampling. Since $\Delta k_y$ is normalized to one, the slope of this function is one. The value $n_{\text{Ref}}$ corresponds to one-half of the base resolution specified in the user interface of the MR scanner. In the example of Figure 4.2, the linear part of the non-Cartesian trajectory runs from zero to $n_{\text{Linear}}$ and is oversampled. The dotted straight line is the extension of this function. Its slope is smaller than the slope of the linear reference function.

This system of equations, Equation 4.5 – Equation 4.8, can be solved to find the expressions for the coefficients of the cubic function of Equation 4.2:

\[
A = \frac{LAF_{\text{Max}} + LAF_{\text{Min}}}{n_{\text{Cubic}}^2} - 2 \cdot \left( \frac{n_{\text{Ref}} - \frac{n_{\text{Linear}}}{OS \cdot AF}}{n_{\text{Cubic}}^3} \right) \quad (4.9)
\]

\[
B = 3 \cdot \left( \frac{n_{\text{Ref}} - \frac{n_{\text{Linear}}}{OS \cdot AF}}{n_{\text{Cubic}}^2} \right) - 2 \cdot \frac{LAF_{\text{Min}} + LAF_{\text{Max}}}{n_{\text{Cubic}}} \quad (4.10)
\]

\[
C = LAF_{\text{Min}} \quad (4.11)
\]

\[
D = \frac{n_{\text{Linear}}}{OS \cdot AF} \quad (4.12)
\]
The properties of the trajectory for a pMRI acquisition are controlled by the choice of the number of linearly sampled data lines ($n_{\text{Linear}}$), the oversampling factor ($OS$) of the linear part of the trajectory, the maximum local acceleration factor ($LAF_{\text{Max}}$) of the non-linear part of the trajectory, and finally the overall acceleration factor ($AF$).

4.2.3 1D non-Cartesian pMRI $k$-space reconstruction

There are two primary ways to perform a 1D non-Cartesian pMRI reconstruction in $k$-space. The first possibility is to reconstruct the data directly onto a Cartesian grid, which fulfills the Nyquist criterion, as depicted on the left side of Figure 4.3. From a pair of acquired non-Cartesian lines, termed source lines, several Cartesian $k$-space lines are reconstructed. Each reconstructed line with a different distance, or a different shift, from the source lines. In the example shown here, three Cartesian $k$-space lines are reconstructed. This procedure is advantageous in that it is not necessary to regrid the data; instead one can use a conventional fast Fourier-Transformation (FFT) to obtain the final image from the reconstructed Cartesian $k$-space. The disadvantage of this procedure is that for each Cartesian $k$-space line a corresponding set of reconstruction parameters for the different shifts, the coil weights, has to be calculated. In other words, for a reconstructed Cartesian data set with $n_{\text{Ref}}$ number of lines, it is necessary to calculate $n_{\text{Ref}}$ sets of coil weights.
In the second approach, the number of coil weights which have to be calculated can be reduced significantly. The basic idea, as depicted on the right side of Figure 4.3, is to reconstruct data lines exactly in between the two measured non-Cartesian source lines. The resulting non-Cartesian data set is used in a second reconstruction step. All measured and reconstructed lines from the first reconstruction step now serve as source lines for the second step. This process is repeated until the non-Cartesian $k$-space fulfills the Nyquist criterion everywhere. Since the source lines are placed symmetrically around the line to be reconstructed in each reconstruction step, it is now possible to interpolate arbitrary coil weights from a small number of calculated coil weights. This

Figure 4.3: Schematic depiction of different reconstruction schemes for a 1D non-Cartesian acquisition: (left) Direct reconstruction of $k$-space lines (dashed lines on the left side) onto a Cartesian grid using acquired non-Cartesian undersampled $k$-space lines (solid lines). In this example, it is necessary to reconstruct three Cartesian lines from two acquired non-Cartesian $k$-space lines to fulfill the Nyquist criterion. (right) In the second approach, two iterations are necessary to fulfill the Nyquist criterion. In a first step, a $k$-space line exactly in the middle of two acquired non-Cartesian lines is reconstructed (indicated by arrows in the 1st reconstruction step). In the second step, acquired (solid lines) and reconstructed lines (dashed lines) from the 1st step are used to reconstruct further lines in between. This figure is reprinted from Reference [38].
A Fast Method for 1D Non-Cartesian Parallel MRI

method can be used as long as the function of the coil weights versus the shift is a smooth function.

4.2.4 1D non-Cartesian GRAPPA coil weights

A modified GRAPPA algorithm was developed for the non-Cartesian pMRI reconstructions of this study. As depicted on the left side of Figure 4.4, a reconstruction must be performed only at positions where the $LAF$ is greater than one (indicated by dashed lines). In general, it is necessary to obtain coil weights for a range of shifts from one-half of the $LAF_{\text{Min}}$ to one-half of the $LAF_{\text{Max}}$, which corresponds to the beginning and the end of the non-linear trajectory. After the first reconstruction step, the former $LAF_{\text{Min}}$ value of 1.5 from Figure 4.4 is reduced to 0.75; no further reconstruction is needed at this position. To fulfill the Nyquist criterion at the outermost position corresponding in this example to a $LAF_{\text{Max}}$ of 4.84, three iterations are needed in total.

The coil weights are derived from the ACS data set similar to [19],[52] using a Moore-Penrose pseudoinverse. All the data acquired within the linear portion of the trajectory serve as original ACS data. Since these ACS data are sampled with a specific density corresponding to a specific sampling distance, only coil weights for shifts identical to this distance or at least multiple integers of this distance could be calculated. ACS data with a smaller distance between adjacent lines are needed to calculate coil weights for a range of shifts in smaller steps than the distance of the original ACS data lines. This can be realized retrospectively by an interpolation of the original ACS data onto a Cartesian grid with smaller distance. Interpolation was performed by zero-filling the low resolution ACS image by a certain factor, followed by an FFT. For the results presented in this study, a zero-filling factor of ten was used.
To improve the accuracy of the reconstruction process, an enlarged GRAPPA kernel as proposed in [52],[53] was used. As depicted on the left side of Figure 4.4, besides the two nearest source points along the phase-encoding (PE) direction, the next neighbors of the source points along the readout (RO) direction are also included in the kernel. In this example, a 2 x 3 GRAPPA kernel, resulting in six source points (black points), is used to reconstruct a single target point (white point). The source points are placed symmetrically around the target point along the PE direction. This is important to make an interpolation of coil weights with arbitrary shifts possible. Since non-Cartesian
sampling is performed along the PE direction, only the two adjacent source points in this direction can be used, otherwise the source points are not distributed symmetrically around the target point. Therefore, the kernel can only be enlarged along the read out direction. For most of the examples shown in this study, a 2 x 5 GRAPPA kernel was used. The basic idea behind the enlarged GRAPPA kernel is to include more information into the fit procedure, which will improve the accuracy of the fit. Assuming an eight element coil array and a 2 x 3 GRAPPA kernel, the coil weight set is made up of 48 values, namely 8 x 2 x 3. As an example, on the right side of Figure 4.4, the real part of the complex coil weight versus a shift from zero to 2.5 is plotted in steps of 0.1. Here, CW(1,48) indicates that data multiplied by this coil weight, together with data multiplied by the other 47 coils weights, will result in reconstructed data from the 1st coil. The set of coil weights for a certain shift is an (8 x 48) matrix, or more general a (NC x NCW) matrix, where NC is the number of coil elements and NCW is the number of coil weights. Instead of performing this fit for each single data point, the source points for all target points are stacked together. This results in two source lines which are three times longer than before, when a 2 x 3 GRAPPA kernel was used. Depending on the size of the interpolated ACS data set and the shift, several fits can be performed along the PE direction. The enlarged source lines and the target lines for all possible positions along the PE direction in the interpolated ACS data set are stacked together to form the final source and the final target lines which are used to estimate an averaged set of coil weights.
4.2.5 Imaging experiments

Imaging studies were performed on a 1.5 T and a 3.0 T whole body scanner (Magnetom Avanto and Magnetom TIM Trio, Siemens Medical Solutions, Erlangen, Germany). For signal reception a 12 channel receive-only head coil array and body coil array was used (Head Matrix and Body Matrix, Siemens Medical Solutions, Erlangen, Germany).

A 1D non-Cartesian FLASH and a 1D non-Cartesian spin echo sequence were developed and implemented on the MR scanners using the IDEA software (Siemens Medical Solutions, Erlangen, Germany).

Healthy volunteers were examined and informed consent was obtained before each study. The following MR imaging protocol was used:

- **FLASH:** \( T_R = 250 \) ms, \( T_E = 5.2 \) ms, alpha = 70°, slice thickness 3.0 mm, FOV 220 mm, image matrix = 256 x 256.
- **SE:** \( T_R = 300 \) ms, \( T_E = 15 \) ms, slice thickness 3.0 mm, FOV 220 mm, image matrix = 256 x 256.

Image reconstruction was performed off-line using the Matlab programming environment (The Mathworks, Natick, MA, USA) installed on a conventional PC with a 2.66 GHz Pentium IV processor and 512 MByte RAM.
4.3 Results

In order to investigate the feasibility of the proposed 1D non-Cartesian pMRI method, several phantom and in vivo studies were performed.

A plot of the positive part of the trajectory which was used for this study is shown on the left side of Figure 4.5.

Figure 4.5: k-space trajectory plots and corresponding local acceleration factors: (left) The graph shows corresponding Cartesian (dashed lines) and non-Cartesian (solid curves) trajectories for different overall net acceleration factors. The Cartesian and the non-Cartesian trajectories cover the same k-space range, which is indicated by the horizontal dashed black line. All trajectories reach this k-space position at 127 $\Delta k_y$. (right) The plot of the corresponding local acceleration factors show that the Cartesian $AF$ (dashed lines) is constant everywhere, while all non-Cartesian trajectories have an oversampled region near the center of k-space, but have higher local acceleration factors in the outer parts. For better visualization, only the positive part of the trajectories is plotted. This figure is reprinted from Reference [38].
In Figure 4.5, the non-Cartesian trajectories (solid curves) for an overall net $AF$ of one, two and four are plotted with their corresponding Cartesian trajectories (dashed lines) which have exactly the same number of sampling points as the non-Cartesian trajectories. In other words, there are no ACS lines included in those trajectories. For the Cartesian GRAPPA acquisition used in this study, a VD sampling scheme was used, which means that additional ACS lines have to be incorporated in the trajectory. The Cartesian and the non-Cartesian trajectories cover the same $k$-space range; the resolution is preserved, shown by the black dashed line at the position $128 \Delta k_y$. As can be seen from the plot of the local acceleration factor (right side of Figure 4.5), all non-Cartesian trajectories have an oversampled region at the beginning, they stay below an $AF$ of one, which is indicated by a dashed blue line.

![Figure 4.6: Direct comparison between non-Cartesian and Cartesian GRAPPA: Non-Cartesian GRAPPA (a-d) and Cartesian GRAPPA (e-h) with a net $AF$ from one to four (from left to right). This figure is reprinted from Reference [38].](image-url)
A direct comparison between Cartesian and non-Cartesian GRAPPA reconstructions is shown in Figure 4.6. In the top row of Figure 4.6 contains non-Cartesian GRAPPA reconstructions. Figure 4.6a is the non-Cartesian reference image without acceleration, while Figure 4.6b –Figure 4.6d show the images of a non-Cartesian GRAPPA reconstruction with overall net acceleration factors of two, three and four. The same is performed for the Cartesian GRAPPA reconstruction in the bottom row of Figure 4.6. Corresponding difference images of this phantom study between the reconstructed images and the reference image are shown in Figure 4.7.

Figure 4.7: Scaled difference images corresponding to the reconstructions of Figure 4.6: (a-c) The difference images between the reference image (from Figure 4.6a) and the non-Cartesian GRAPPA reconstructions with a net $AF$ of 2, 3 and 4 (from Figure 4.6b –Figure 4.6d). (d-f) The difference images of the Cartesian reconstructions. It is obvious that for higher acceleration factors the non-Cartesian difference image (c) shows significantly reduced residual artifacts compared to the Cartesian difference image (f). This is also reflected in the RMS error values listed in Table 4.2. This figure is reprinted from Reference [38].
Figure 4.8: Cartesian versus non-Cartesian reconstructions for a net acceleration factor of four: (a) The five ROIs corresponding to the SNR values listed in Table 4.3 are indicated. (b) Image profiles, through a section of the Cartesian (dashed curve) and the non-Cartesian (solid curve) reconstruction. (c,d) Cartesian (c) and non-Cartesian (d) noise map. (e,f) Cartesian (e) and non-Cartesian (f) difference images. This figure is reprinted from Reference [38].
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Figure 4.8 highlights different properties of the Cartesian and the non-Cartesian reconstructions for a net acceleration factor of four. Besides image profiles (Figure 4.8b), and noise maps (Figure 4.8c and Figure 4.8d), difference images between a full FOV reference and the reconstructions (Figure 4.8e and Figure 4.8f) are shown.

Finally, in vivo examples using a non-Cartesian FLASH sequence and a non-Cartesian Spin-Echo sequence are shown in Figure 4.9.

![Figure 4.9: Comparison between Cartesian and non-Cartesian GRAPPA in vivo acquisitions with an overall net $AF$ of 3: (top row) $T_1$ weighted spin-echo acquisitions. (a) Cartesian reference image. (b) Cartesian GRAPPA reconstruction with a net $AF = 4$ using 48 ACS lines. (c) The non-Cartesian GRAPPA reconstruction shows no residual artifacts, here the $LAF_{max}$ was 4.43. (bottom row) $T_1$ weighted FLASH acquisitions: (d) Cartesian reference image. (e) Cartesian GRAPPA reconstruction with a net $AF = 4$ using 19 ACS lines. (f) The non-Cartesian GRAPPA reconstruction shows no residual artifacts, here the $LAF_{max}$ was 4.43. Both Cartesian GRAPPA reconstructions show residual artifacts, which are highlighted by arrows. Due to a slightly different breath hold position this slices is not exactly the same as (d) and (e). This figure is reprinted from Reference [38].]
4.4 Discussion

The non-Cartesian trajectory used for this study was optimized to acquire a sufficient number of ACS lines and to cover exactly the same $k$-space range as a corresponding Cartesian trajectory for comparison. However, other 1D non-Cartesian trajectories can be designed for different purposes [21], [39]-[43], as for example, to improve the point-spread-function [43]. For all non-Cartesian acquisitions, 21 ACS lines, including the center line, were acquired with the linear part of the trajectory. Those lines were acquired at the Nyquist sampling rate, but it is also possible to oversample this region slightly to make the calculation of the coil weights more robust. Whenever the FOV is chosen to be too small, prefolding artifacts would appear in the ACS image and interpolation via zero-filling in the image domain, or an interpolation directly in $k$-space will fail. An oversampling of the center of $k$-space makes the reconstruction more robust by preventing possible prefolding.

There are some important differences between the Cartesian and the non-Cartesian GRAPPA acquisitions, which are listed in Table 4.1. The values listed in Table 4.1 were used for the phantom study assuming a 256 x 256 image matrix with a square FOV. Slightly different values were used for the in vivo abdominal acquisitions (see Figure 4.9) because a rectangular FOV was used. To achieve a certain overall net acceleration factor for Cartesian GRAPPA, it is necessary to acquire the data using a higher acceleration factor. This is due to the fact that in the VD-sampling approach, the ACS lines and the actual accelerated data are acquired in the same scan. In other words, to achieve a net acceleration factor of two for a Cartesian GRAPPA acquisition, it is necessary to acquire the data with an $AF$ of three and 80 ACS lines in the
center. In comparison, 21 ACS lines were always used for the non-Cartesian GRAPPA acquisitions in this study, but different $LAF_{\text{Max}}$ values were chosen. As mentioned in the introduction, the VD-approach is only one possible realization of the autocalibration. It is also possible for Cartesian and non-Cartesian GRAPPA to acquire the ACS data before or after the actual accelerated data. In this case, the $LAF_{\text{Max}}$ in the non-Cartesian acquisition could be reduced.

<table>
<thead>
<tr>
<th>pMRI</th>
<th>net $AF = 2$</th>
<th>net $AF = 3$</th>
<th>net $AF = 4$</th>
</tr>
</thead>
<tbody>
<tr>
<td>Cartesian</td>
<td>$AF = 3$</td>
<td>$AF = 4$</td>
<td>$AF = 5$</td>
</tr>
<tr>
<td>(GRAPPA kernel 4 x 5)</td>
<td>80 ACS</td>
<td>48 ACS</td>
<td>24 ACS</td>
</tr>
<tr>
<td>non-Cartesian</td>
<td>$LAF_{\text{Max}} = 2.64$</td>
<td>$LAF_{\text{Max}} = 4.43$</td>
<td>$LAF_{\text{Max}} = 6.56$</td>
</tr>
<tr>
<td>(GRAPPA kernel 2 x 5)</td>
<td>21 ACS</td>
<td>21 ACS</td>
<td>21 ACS</td>
</tr>
</tbody>
</table>

Table 4.1: Differences between Cartesian and non-Cartesian GRAPPA acquisitions: Here the different conditions to achieve a certain overall net acceleration factor are listed, assuming an image matrix of 256 x 256 with a square FOV.

For all reconstructions with a base resolution of 256, only 30-65 sets of coil weights were calculated. For a non-Cartesian GRAPPA reconstruction with the same base resolution, 256 sets of coil weights would be necessary to reconstruct all the missing data. Using the calculated sets of coil weights, additional sets of coil weights for arbitrary shifts were derived by interpolation. This means that with our approach of interpolating coil weights, the number of weights which must be calculated is reduced by a factor of four to eight for the examples shown in this study. Since the calculation of the coil weights is the most time consuming procedure in the whole pMRI reconstruction, this reduction of the number of coil weights is essential. To further speed up the reconstruction process it is possible to reduce the size of the GRAPPA kernel. A 2 x 5 GRAPPA kernel was used for all non-Cartesian reconstructions in this study because it provides the best image quality for all acceleration factors.
tested, and it provides reconstruction times comparable to Cartesian GRAPPA reconstructions with a 4 x 5 GRAPPA kernel. For a net $AF$ of two, it is possible to speed up the reconstruction process, simply by using a 2 x 3 GRAPPA kernel, without any noticeable loss in image quality. This is not the case for higher acceleration factors; for example, for a net $AF$ of four such a smaller kernel results in a reduced image quality. On the other hand, reconstructions with a larger kernel size than 2 x 5 will only marginally improve the overall image quality of the reconstruction, but will drastically increase the reconstruction time (depending upon the CPU and the memory of the computer system.)

The time necessary to calculate the coil weights for a net $AF$ of two decreases from 8 s to 3 s when the kernel size is reduced from a 2 x 5 kernel to a 2 x 3 kernel. In comparison, the time necessary to calculate the weights in Cartesian GRAPPA with a 4 x 5 kernel and 80 ACS lines is 21 s. Of course, such a large numbers of ACS lines are generally not employed in conjunction with VD-sampling. One would instead use between 20 and 30 ACS lines for an $AF$ of two, resulting in a net $AF$ of about 1.8. The time necessary to calculate the weights would be between 5 s and 8 s, which is comparable to the time needed to calculate the weights for the non-Cartesian case.

For the reconstruction of the missing data, the situation is different. The non-Cartesian reconstruction takes about 15 - 25 s depending on the kernel size, while in the Cartesian case it is about 8 s. The non-Cartesian reconstruction also includes the direct Fourier Transformation, which takes about 6 s to compute. Here, the Cartesian reconstruction is faster and takes about 8 s. Those numbers should not be treated as absolute values; they can only provide a rough benchmark, as reconstruction times strongly depend upon the computer hardware and the software used for calculations.

Compared to the reconstruction times, it is easier to measure the image quality, for example by using the root-mean-square (RMS) error, the SNR, and the
artifact power. The results of those measures are listed in Table 4.2 and Table 4.3. As can be seen from the RMS values for the phantom study (see Table 4.2), the non-Cartesian and the Cartesian GRAPPA reconstructions show similar results for net acceleration factors of two and three. For a net acceleration factor of four, the non-Cartesian reconstruction is clearly beneficial, as the RMS error of the Cartesian GRAPPA reconstruction is nearly twice as big as for the non-Cartesian. This behavior is visible in the reconstructed images shown in Figure 4.6 and the scaled difference images shown in Figure 4.7.

<table>
<thead>
<tr>
<th>net AF</th>
<th>Cartesian</th>
<th>non-Cartesian</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>1.4 %</td>
<td>1.3 %</td>
</tr>
<tr>
<td>3</td>
<td>2.7 %</td>
<td>2.6 %</td>
</tr>
<tr>
<td>4</td>
<td>16.8 %</td>
<td>8.6 %</td>
</tr>
</tbody>
</table>

Table 4.2: Comparison between Cartesian and non-Cartesian GRAPPA reconstructions: Root-mean-square error of Cartesian and non-Cartesian GRAPPA reconstructions for different net acceleration factors.

To further investigate the overall image quality, the resolution and the noise behavior are examined. In Figure 4.8b, plots of an image profiles are shown. It is clear from Figure 4.8 that the Cartesian (blue plot) and the non-Cartesian (red plot) reconstruction show a similar resolution. The major differences in the two plots arise from residual fold-over artifacts from the Cartesian GRAPPA reconstruction, but this does not manifest itself in a different resolution.

More difficult to quantify is the SNR behavior. As described in [44] the difference of two images acquired directly after each other is an adequate method to derive the SNR at least for phantom studies, which are not affected by any kind
of motion. The advantage of this method is that it can also be used for phased array coils, as the use of the difference of two images eliminates difficulties arising from the non-uniformity of the coil sensitivities. However, the situation is much more complex when parallel imaging must be taken into account. As can be seen in the noise maps (see Figure 4.8c and Figure 4.8d) the noise enhancement is different for Cartesian and non-Cartesian GRAPPA reconstructions for a net acceleration factor of four. The overall level of additional noise from the reconstruction seems to be comparable for both cases, but the distribution of the noise is quite different. This can be seen by comparing the SNR for different regions of interest (ROIs), as listed in Table 4.3 (the ROIs are highlighted in Figure 4.8a.) ROI I – IV show similar values for both methods, but in ROI V the SNR for the Cartesian GRAPPA is nearly twice as large as the SNR for the non-Cartesian GRAPPA.

<table>
<thead>
<tr>
<th>ROI</th>
<th>Cartesian</th>
<th>non-Cartesian</th>
</tr>
</thead>
<tbody>
<tr>
<td>I</td>
<td>41</td>
<td>47</td>
</tr>
<tr>
<td>II</td>
<td>54</td>
<td>45</td>
</tr>
<tr>
<td>III</td>
<td>40</td>
<td>35</td>
</tr>
<tr>
<td>IV</td>
<td>60</td>
<td>67</td>
</tr>
<tr>
<td>V</td>
<td>117</td>
<td>75</td>
</tr>
</tbody>
</table>

Table 4.3: Comparison between Cartesian and non-Cartesian GRAPPA reconstructions: Calculated SNR of different ROIs (see Figure 4.8a) for a net acceleration factor of four.
In the non-Cartesian reconstruction, the region of additional noise arising from the reconstruction process is broader compared to the Cartesian case. Due to the reconstruction-based additional noise contribution, the SNR can be significantly different for adjacent ROIs, even when coil sensitivity variations are accounted for and a homogenous object is imaged. In general, there is a trade of between SNR and reduction of remaining aliasing artifacts. In the special case of non-Cartesian pMRI with high acceleration factors presented in this study, this loss in SNR is obviously more than compensated by the reduction of the severe aliasing artifacts.

On the other hand the artifact power, as described in [45], is a global quantity of error in the reconstruction since in addition to the noise due to the pMRI reconstruction it also takes remaining fold-over artifacts into account. Here, the benefit of the non-Cartesian GRAPPA strategy is visible. Compared to an artifact power of 2.9 % for the Cartesian GRAPPA, the artifact power for the non-Cartesian strategy is only 1.5 %. This behavior is visible in the difference images shown in Figure 4.8e and Figure 4.8f. Here, the Cartesian/non-Cartesian GRAPPA reconstructions are subtracted from a full FOV Cartesian/non-Cartesian reference image.

Finally, in vivo examples using a non-Cartesian spin-echo sequence and a non-Cartesian gradient-echo sequence are shown in Figure 4.9. An overall net acceleration factor of 3 was obtained for the Cartesian/non-Cartesian GRAPPA acquisitions. Remaining fold-over artifacts in the Cartesian GRAPPA images (highlighted by arrows in Figure 4.9b and Figure 4.9e) are clearly suppressed in the non-Cartesian GRAPPA reconstructions (Figure 4.9c and Figure 4.9f).
4.5 Summary

In this chapter, a new approach for 1D non-Cartesian fast GRAPPA reconstructions has been presented. For this study, gradient echo and spin echo sequences using an optimized trajectory for 1D non-Cartesian autocalibrated pMRI were developed. Results from phantom and in vivo experiments were shown and compared to Cartesian GRAPPA reconstructions. Compared to previous $k$-space based non-Cartesian pMRI methods, the reconstruction time is in the range of the time required for Cartesian pMRI reconstructions. In addition to this improvement, the non-Cartesian GRAPPA approach presented in this study shows better results for high acceleration factors than a corresponding Cartesian GRAPPA reconstruction.
5 A Direct Method for Spiral Parallel MRI

5.1 Introduction

In the last chapter, a fast pMRI reconstruction method for undersampled 1D non-Cartesian sampled MR data using the GRAPPA technique was introduced. It was shown that the more relaxed fold-over artifact behavior of the 1D non-Cartesian trajectory is advantageous, especially for high acceleration factors.

In this chapter, the pMRI reconstruction approach is extended to two dimensional undersampled non-Cartesian data. Therefore, a new reconstruction concept is derived compared to the 1D case.

In the past, pMRI reconstructions of 2D non-Cartesian sampling schemes, such as spiral trajectories, have been reported to require several hours and sometimes even days to reconstruct the images from a typical fMRI investigation [54]-[58]. Whereas these previous investigations have performed the reconstruction using coil sensitivity information from the image domain, recent approaches for parallel imaging of non-Cartesian $k$-space sampling by means of the GRAPPA algorithm [19], work completely in $k$-space and represent a promising approach to overcome computational limits [59].
In this chapter, a new reconstruction algorithm for pMRI of non-Cartesian spiral trajectories is introduced. The algorithm is based on the GRAPPA methodology and allows the full reconstruction of accelerated data with a computational effort comparable to Cartesian pMRI. Application of pMRI in fast spiral imaging can considerably improve image quality through, for example, reduced blurring [57] and enables high image quality in single-shot spiral images with high spatial resolution (1x1 mm² in plane resolution). Potential applications that will benefit from the improved image quality and/or improved temporal resolution by the proposed method range from high resolution functional MRI investigations, arterial spin labeling techniques, and diffusion imaging to cardiac applications with spiral readout trajectories.

5.2 Theory and Methods

5.2.1 Spiral trajectories

For all acquisitions and calculations in this study, closed form approximate solutions of Archimedean spirals were used [65]. The \( k_x, k_y \)-trajectories of these spirals can be described by the following formulas:

\[
k_x(I_{\text{actual}}, t) = a \cdot \tau(t) \cdot \cos(2 \cdot \pi \cdot w \cdot \tau(t) + (I_{\text{actual}} - 1) \cdot \left(\frac{-2 \cdot \pi}{I_{\text{total}}}\right)) \quad (5.1)
\]

\[
k_y(I_{\text{actual}}, t) = a \cdot \tau(t) \cdot \sin(2 \cdot \pi \cdot w \cdot \tau(t) + (I_{\text{actual}} - 1) \cdot \left(\frac{-2 \cdot \pi}{I_{\text{total}}}\right)) \quad (5.2)
\]

The number of rotations or windings of the spiral is given by \( w \). The parameter \( a \), an integer, is the maximum \( k \)-space radius in multiples of \( \Delta k \) and determines the resolution of a spiral acquisition.
As shown on the left side of Figure 5.1, $\Delta k$ is the radial distance between two adjacent windings and is usually determined by the Nyquist criterion to avoid undersampling. In this figure, the maximum $k$-space radius is eight $\Delta k$, which is achieved in four windings with a single interleaf. The same resolution with essentially the same sampling density can be obtained in a single winding when four interleaves are used. The initial angle of an interleaf is determined by the phase term in Equation 5.1 and Equation 5.2, where the variable $I_{\text{actual}}$ is the number of the actual interleaf which varies from one to $I_{\text{total}}$, the total number of interleaves used for the acquisition. For data acquisition along the spiral trajectory, the parameter $\tau(t)$ in Equation 5.1 and Equation 5.2 is a function of the time $t$ and of the gradient performance and is normalized to one. For spirals

**Figure 5.1:** Single-shot and multi-shot spiral trajectories: (left) A single interleaf $I_1$ is used for single-shot spiral imaging. The radial distance $\Delta k$ between the windings of the spiral is determined by the maximum $k$-space radius $a$ and the number of windings $w$. In this example, $a=8$ and $w=4$. (right) The same $k$-space coverage with essentially the same sampling density can be obtained in a single winding by using four interleaves. In both cases, the first interleaf $I_1$ (solid line) starts with an initial angle of zero degrees. When more interleaves are used, the initial angles are distributed equally over the whole range of 360°. This figure is reprinted from Reference [64].
running from the center outwards (spiral out), $\tau(t)$ runs from zero, with the acquisition of the center point, to one, the acquisition of the outermost point, in a pre-defined step size. For the special case that $\tau(t) = t$, the amount of time which is spent for each winding is constant, regardless of whether the acquired winding is near the center or in the outer part of the spiral. In other words, the readout gradients reach their maximum performance at the end of the acquisition. This acquisition scheme, initially proposed by Ahn et al [66], is called constant-angular-velocity spiral trajectory. The constant-angular-velocity spiral trajectory can easily be transformed into a so-called constant-linear-velocity spiral by the choice of $\tau(t) = \sqrt{t}$ in Equation 5.1 and Equation 5.2. It has been shown [67] that the constant-linear-velocity spiral offers some advantages in terms of SNR and gradient performance as compared to the constant-angular-velocity spiral.

Although constant-linear-velocity spiral trajectories are more practical, the constant-angular-velocity spiral trajectories have some interesting properties. In a constant-angular-velocity Archimedean spiral, the number of sampling points per winding is constant. If this number is even, all acquired data points are aligned along straight lines through the origin and are collinear with the center point, as schematically shown in Figure 5.2. Another important property of such a spiral is that the distances in $k$-space between sampled data points along such a line through the origin are constant, except for those points directly adjacent to the central $k$-space point. The symmetry of the constant-angular-velocity spiral, which is similar to the symmetry of a radial trajectory, was used by Ahn et al [66] to reconstruct the first spiral images with a convolution-backprojection algorithm. To emphasize the similarity to radial acquisitions, data points collected along these lines are further called pseudo-projections. The fast pMRI approach for spiral imaging presented in this chapter also makes use of the high symmetry of a constant-angular-velocity trajectory. To benefit from the
advantages of a constant-linear-velocity trajectory, the acquisition is performed with this trajectory, while the pMRI reconstruction is performed with the data interpolated onto a constant-angular-velocity spiral trajectory.

**Figure 5.2:** Properties of constant-angular-velocity spiral trajectories: The number of acquired data points per winding for this trajectory is constant. Data points acquired or interpolated onto a constant-angular-velocity spiral trajectory, indicated by gray points, lie on straight lines through the origin and are collinear with the center point (black point). In this example, the number of data points per winding is eight, which can be collected in four pseudo-projections $P_1 - P_4$ (gray lines). In contrast to a radial acquisition, the center point is identical for all pseudo-projections, and the distance between points adjacent to the center point is not constant. This figure is reprinted from Reference [64].
5.2.2 Interpolation of data along the spiral trajectory

Since the only difference between the constant-linear-velocity and constant-angular-velocity trajectories is a change of trajectory along the time axis, and not a change in overall $k$-space coverage, only a simple one-dimensional interpolation along the time dimension is required. This is advantageous because it avoids the problem of a two-dimensional interpolation directly in $k$-space, since there is not enough information to perform this interpolation for the undersampled trajectories used here. A depiction of the 2D and 1D interpolation is shown in Figure 5.3. A simple 2D interpolation between two adjacent data points (gray points in Figure 5.3) in $k$-space will result in a position which is no longer part of the spiral trajectory (see white square in Figure 5.3). Compared to this, the specific time stamp of a 1D interpolation along the time dimension is always related to the specific $k$-space data point on the spiral trajectory (white point).

![Figure 5.3: Interpolation in 2D $k$-space and 1D time dimension: (left) A simple interpolation exactly in between two adjacent data points (grey points) in $k$-space will lead to a wrong position (white square). The interpolated data point is no longer part of the spiral trajectory. (right) Since the spiral trajectory is defined by the timing, an interpolation between two adjacent data points along the 1D time dimension will always result in a data point which is part of the spiral trajectory (white point). This figure is reprinted from Reference [64].](image-url)
For the 1D interpolation from a constant-linear-velocity spiral trajectory onto a constant-angular-velocity trajectory it is only necessary to know the timing of both the original and the target trajectory.

Assuming that the timing is identical for each interleaf, the timing of the constant-linear-velocity (the original trajectory) can be calculated from the $k_x, k_y$ trajectory information by solving Equation 5.1 and Equation 5.2 for the time function $\tau(t)$.

$$\tau(t) = \frac{\text{unwrap} \left( \arctan \left( \frac{k_y(I_{\text{actual}}, t)}{k_x(I_{\text{actual}}, t)} \right) \right)}{2\pi w}$$

(5.3)

Here, $\text{unwrap}$ is a phase unwrap procedure, which adds appropriate multiples of $2\pi$ to each phase input to restore the original phase values. As stated earlier, the timing of the constant-angular-velocity trajectory (the target trajectory) is simply $\tau(t) = t$.

### 5.2.3 Reordering of $k$-space data into a new hybrid space

After interpolation of the data onto a constant-angular-velocity spiral trajectory, the next step is to exploit the high symmetry of this trajectory to fast pMRI reconstructions. A simple way to potentially do this is depicted in Figure 5.4.

Data points acquired or interpolated onto such a spiral trajectory can be regrouped in pseudo-projections. In contrast to the projections of a radial acquisition, the pseudo-projections $P_1$-$P_4$ in Figure 5.4 all share the same central $k$-space point, since it is only acquired once per interleaf in a spiral acquisition. Further, the distance between the data points adjacent to the central
$k$-space point is not constant. Due to these inherent asymmetries, this choice of pseudo-projections can be a problem for pMRI reconstructions.

Different pseudo-projections without these problems can be obtained by simply changing the data points which constitute the pseudo-projection. The pseudo-projections, shown on the left side of Figure 5.4, all start with the corresponding point of the first winding of the spiral and do not share the center point. In addition, there are now twice as many pseudo-projections (here $P_1 – P_8$). Compared to the pseudo-projections shown in Figure 5.3, the distance between measured data points is now constant, resulting in a more symmetric reconstruction.

After specification of the pseudo-projections, the next step is to reorder these projections from the $k_x,k_y$ space into a new hybrid space enabling a pseudo-Cartesian GRAPPA reconstruction of the data. This process can be facilitated by rearranging the spiral $k$-space data into a new hybrid space with coordinates winding ($w$) and projection angle ($\Phi$), which is shown schematically on the right side of Figure 5.4. In this hybrid-space, the distance between data points in both directions is constant. This approach is similar to the radial GRAPPA approach described in [59], where data points on missing projections between measured projections are reconstructed in a radius ($r$) projection angle ($\Phi$) hybrid space. In comparison to the radial approach where the reconstruction is performed between different projections, the spiral GRAPPA reconstruction is performed along a single pseudo-projection. In other words, the orthogonal problem has to be solved.
Figure 5.4: Depiction of the reordering scheme for undersampled constant-angular-velocity spiral data with two interleaves. Solid lines represent measured data from the first interleaves, dashed lines indicate missing data from the second interleaves: (top, left) Measured data points (indicated by black and gray points) are collected in pseudo-projections (here P1 – P8), which all start with a point from the first winding of the first interleaves (black points). (top, right) Reordering is performed by simply rearranging the spiral data winding by winding in the new winding (W) projection angle (Φ) hybrid space. The first measured data line in this hybrid space starts with the center point in the lower left corner and contains all measured points of the first winding of the spiral (black points). In the same manner, the second measured data line starts with the first point of the second winding and contains all measured points of the second winding of the spiral (gray points). In this scheme, each data line or winding starts with a point from projection P1, which is indicated by bigger points. (bottom) The segmentation of the hybrid space (bottom, right) corresponds to a division of the spiral trajectory into sectors (bottom, left). This figure is reprinted from Reference [64].
5.2.4 Modified GRAPPA Reconstruction

All spiral pMRI reconstructions in this chapter were performed with a modified Cartesian GRAPPA algorithm [19]. This autocalibrated pMRI method has the advantage that it does not rely upon accurate coil sensitivity information. Instead, some fraction of the data is acquired without undersampling, which can be done before, after or during the actual accelerated acquisition. These so-called autocalibration signals (ACS) are used to derive the pMRI reconstruction parameters directly in $k$-space by a fitting procedure [17]-[19]. For each study, several repetitions without undersampling were acquired. In general, a fully sampled spiral data set served as ACS signal, while the spiral GRAPPA reconstruction was performed on undersampled spiral data sets from different repetitions.

The pMRI reconstruction scheme used for this study is depicted in Figure 5.5. As shown on the left side of Figure 5.5, several measured data points along the pseudo-projection $P_2$ are used as source points (black points) to reconstruct a single missing data point, called the target point (white point). With the above described reconstruction scheme using four source points along the pseudo-projection, it would not be possible to reconstruct all missing data in the hybrid space. At the edges of the hybrid space, it is not possible to reconstruct the outermost missing data points. Therefore, it is necessary to modify the reconstruction scheme by simply using a shifted target point position. The target point can be located at the center position, as shown on the left side of Figure 5.5, or at any other position (indicated by bright gray points in Figure 5.5). It is not necessary that the source points are placed symmetrically around the target point. With the new position of the target point, new reconstruction parameters have to be calculated.

For all examples in this study, we have used four source points along the pseudo-projection. More source points will increase the reconstruction times.
with only minimal improvement of image quality. To improve the accuracy of the fit, additional source points from neighboring pseudo-projections (P₁ and P₃) are incorporated into the reconstruction process, which is shown schematically on the right side of Figure 5.5.

The arrangement of source points is termed the reconstruction kernel. For all examples shown in this study, a 4 x 3 reconstruction kernel with 4 source points
along the pseudo-projection and 3 neighbored projections was used. Instead of performing the fit for each pseudo-projection, the reconstruction is improved by using several pseudo-projections to estimate an averaged set of reconstruction parameters. This is accomplished by dividing the hybrid data set into segments along the $\Phi$ direction, which corresponds to a division of the spiral trajectory into sectors. This segmentation process is depicted on the bottom of Figure 5.4 using 4 segments in the hybrid space, in other words, 4 sectors in $k$-space. For each sector, averaged reconstruction parameters are derived separately; the total number of sectors was 56 for all examples. An additional segmentation along the radial direction was not performed, because it was observed that this does not improve the direct spiral GRAPPA reconstruction.

After reconstructing all missing data points, the complete hybrid space is reordered back into the normal $k_x,k_y$ space onto the spiral trajectory. To obtain the final images, a regridding procedure similar to that described in [68], [69] is applied to the regenerated spiral data set.

5.2.5 Imaging experiments

Imaging studies were performed on a 1.5 T and on a 3.0 T whole body scanner. Informed consent was obtained from all subjects prior to the investigations. The 1.5 T MR-scanner (Magnetom Avanto, Siemens Medical Solutions, Erlangen, Germany) was equipped with 32 independent receiver channels and gradients achieving peak gradient amplitudes of 45 mT/m and a maximum slew rate of 200 T/m/s. For signal reception a prototype 23 channel receive-only head coil array was used. The coil elements were mounted on a closely fitting helmet modeled after the European head standard form EN960/1994 for protective headgear. The coil circumference is 629 mm, 222 mm maximum in AP, 181 mm in RL, and 210 mm in SI. The array consisted of 23 overlapped circular surface
coil elements, 17 with a diameter of approximately 10 cm and 6 with a diameter of approximately 7 cm, arranged in a geodesic tiling over the dome of the head which places groups of circular elements arranged in the soccer ball symmetry at the four “corners” of the head: left and right temple and the corresponding posterior sections and additionally on the vertex. Preamplifier decoupling was used to reduce interactions between the coil elements in addition to nulling mutual inductance between nearest neighbors with coil overlap.

The 3.0 T MR scanner (Magnetom Trio, Siemens Medical Solutions, Erlangen, Germany) was equipped with 32 independent receiver channels and gradients achieving peak gradient amplitudes of 40 mT/m and a maximum slew rate of 200 T/m/s For signal reception, an eight channel product head coil array (MRI Devices, Waukesha, USA) or a 32 channel prototype head array (similar to the 23 channel head coil at 1.5 T) were used.

For all spiral acquisitions the maximum slew rate and gradient amplitude for the readout trajectory were 150 T/m/s and 20 mT/m, respectively. Three healthy volunteers were examined and informed consent was obtained before each study. The following spiral MR imaging protocol was used:

\[ T_R = 2500-3000 \text{ ms}, \quad T_E = 40 \text{ ms (1.5T)}, \quad T_E=3.6 \text{ ms (3.0T)} \text{ and } T_E=30 \text{ ms (3.0T)}, \quad \alpha = 75^\circ, \quad \text{slice thickness } 3.5-4 \text{ mm, FOV 220-240 mm, image matrix } = 192 \times 192 \text{ or } 256 \times 256 \]

The minimum number of windings per interleaf was 12, which corresponds to an eight-interleaves acquisition with an image matrix of 192. The maximum number of windings per interleaf was 128, which corresponds to a single shot acquisition with an image matrix of 256. Image reconstruction was performed off-line using the Matlab programming environment (The Mathworks, Natick, MA, USA) installed on a conventional PC with a 2.66 GHz Pentium IV processor and 512 MByte RAM.
5.3 Results

In order to investigate the influence of the ACS data on the direct GRAPPA reconstruction, several phantom studies were performed. In separate acquisitions, ACS data sets were acquired with different image resolution and different contrast behavior than the acquisitions used for the direct spiral GRAPPA reconstructions. For the study shown in Figure 5.6, a low resolution ACS data set (Figure 5.6a) from a separate acquisition was used to derive the reconstruction parameters. Besides the direct spiral GRAPPA reconstructed image (Figure 5.6d), the fully sampled reference image (Figure 5.6b) and the undersampled image (Figure 5.6c) are shown for comparison. The difference image (Figure 5.6e) between the fully sampled reference image (Figure 5.6b) and the direct spiral GRAPPA reconstruction (Figure 5.6d) with an acceleration factor of two is scaled to the maximum signal of the reference image. In Figure 5.7 an ACS data set with different contrast behavior than the accelerated direct spiral GRAPPA reconstruction was used. This ACS data set was obtained with a short $T_E$ ($T_E = 2.9$ ms), resulting in different signal intensities in some tubes of the ACS image (Figure 5.7a). The fully sampled reference acquisition was obtained with a long $T_E$ ($T_E = 35$ ms). There is a tube in the reference image (Figure 5.7b), which shows a different contrast behavior than in the ACS image. This tube is highlighted by an arrow. In order to show that this tube is placed in a region affected by the undersampling, the undersampled spiral image is shown in Figure 5.7c. As can be seen in the direct spiral GRAPPA reconstruction (see Figure 5.7d) the reconstruction process does not affect the contrast of this tube. This behavior is also visible in the difference image (Figure 5.7e).
Figure 5.6: Direct spiral GRAPPA reconstruction with low resolution ACS data: (a) A low resolution spiral data set of a separate acquisition is used to derive the reconstruction parameters. (b) The fully sampled high resolution reference image and the undersampled spiral image (c) are shown for comparison. (d) The direct spiral GRAPPA reconstruction with an acceleration factor of two. (e) The difference image between the reference image and the direct spiral GRAPPA reconstruction is scaled to the maximum signal of the reference image. The RMS error normalized by the RMS energy of the reference image is 3.5%. This figure is reprinted from Reference [64].
Figure 5.7: Direct spiral GRAPPA reconstruction where the contrast behavior of the ACS data differs from that of the accelerated data: (a) In a separate acquisition a spiral data set was obtained with a short TE serving as ACS data set to derive the reconstruction parameters. (b) The fully sampled reference image obtained with a long TE and the corresponding undersampled spiral image (c) are shown for comparison. (d) The direct spiral GRAPPA reconstruction with an acceleration factor of two. (e) The difference image between the reference image and the direct spiral GRAPPA reconstruction is scaled to the maximum signal of the reference image. The RMS error normalized by the RMS energy of the reference image is 9.5%. This figure is reprinted from Reference [64].
In Figure 5.8, image profile lines through this tube are plotted. As can be seen in this figure, the ACS image profile (red curve) through this tube shows higher signal intensity than those of the reference image (green curve). The image profile line of the spiral GRAPPA reconstruction (black curve) shows the same signal behavior than the reference image profile.

Figure 5.8: Single image profile lines running through a tube (indicated by an arrow in the right image) with different contrast behavior. The position of the profile line is highlighted by the white line in the image on the right side (the reference image from Fig. 5.7. In the tube (indicated by an arrow in the plot), the ACS image profile (red curve) shows a high signal intensity, while the reference (green curve) and the direct Spiral GRAPPA reconstruction (black curve) image profile show both a low signal intensity. This figure is reprinted from Reference [64].
High resolution spiral images with a matrix size of 256 x 256 obtained at 1.5 T with the prototype 23 channel head coil are shown in Figure 5.9. The full acquisition reference images with two to eight interleaves are shown in the left column of Figure 5.9. As can be seen in the middle column of Figure 5.9, images from undersampled spiral data sets using only a single interleaf suffer from severe aliasing artifacts. The corresponding pMRI reconstructions of the undersampled single-shot spiral data sets with acceleration factors from two to eight are shown in the right column of Figure 5.9.
Figure 5.9: High resolution (0.9x0.9x4 mm$^3$) conventional multi-shot spiral versus single-shot spiral GRAPPA examples at 1.5 T, acquired with a 23 channel head array: Full acquisition reference images with two, four and eight interleaves (left column from top to bottom). Only a single interleaf of each spiral data set is used resulting in two-, four- and eight-times undersampled images (center column from top to bottom). Spiral GRAPPA reconstructions with acceleration factors of two, four and eight (right column from top to bottom). This figure is reprinted from Reference [64].
Figure 5.10: High resolution (1.25x1.25x4 mm$^3$) conventional multi-shot spiral versus single-shot spiral GRAPPA examples at 3.0 T, acquired with an eight channel head array: Full acquisition reference images with two, four and eight interleaves (left column from top to bottom). Only a single interleaf of each spiral data set is used, resulting in two-, four- and eight-times undersampled images (center column from top to bottom). Spiral GRAPPA reconstructions with acceleration factors of two, four and eight (right column from top to bottom). This figure is reprinted from Reference [64].
Imaging results obtained at 3.0 T with an eight channel head coil (MRI Devices, Waukesha, USA) are shown in Figure 5.10. As in Figure 5.9, reference images with two to eight interleaves and a matrix size of 192 x 192 are on the left side, the undersampled images are in the middle column, and the corresponding pMRI reconstructions are shown in the right column of Figure 5.10.

High resolution T2* weighted imaging results obtained at 3.0 T with a 32 channel prototype head array are shown in Figure 5.11. As in Figure 5.10, reference images with two to eight interleaves and a matrix size of 256 x 256 are on the left side, the undersampled images are in the middle column, and the corresponding pMRI reconstructions are shown in the right column of Figure 5.11.

Figure 5.12 shows a direct comparison between conventional single-shot spiral imaging with pMRI single-shot spiral T2* weighted imaging at 3.0 T. The conventional single-shot spiral images shown on the left side of Figure 5.12 suffer from severe off-resonance effects. These effects are clearly reduced by the use of single-shot spiral pMRI, which can be seen on the right side of Figure 5.12.
Figure 5.11: High resolution (0.86x0.86x3.5 mm$^3$) $T_2^*$ weighted conventional multi-shot spiral versus single-shot spiral GRAPPA examples at 3.0 T, acquired with a 32 channel prototype head array: Full acquisition reference images with two, four and eight interleaves (left column from top to bottom). Only a single interleaf of each spiral data set is used, resulting in two-, four- and eight-times undersampled images (center column from top to bottom). Spiral GRAPPA reconstructions with acceleration factors of two, four and eight (right column from top to bottom). This figure is reprinted from Reference [64].
Figure 5.12: High resolution (0.86x0.86x3.5 mm³) T₂* weighted single-shot spiral acquisitions at 3.0 T, acquired with a 32 channel prototype head array. Especially in basal regions of the brain, the conventional single-shot spiral acquisition suffers from severe off-resonance artifacts (left column). The single-shot spiral GRAPPA acquisition with acceleration factor of eight shows a significantly improved off-resonance behavior (right column). Two different slices from a healthy volunteer are shown in the top and the bottom row. This figure is reprinted from Reference [64].
5.4 Discussion

Off-resonance effects can severely affect image quality in spiral imaging. Since these effects scale with the readout duration, the common solution to this problem is to reduce the readout length. Without undersampling of $k$-space, this can be realized by using stronger gradients or several interleaves with increased total acquisition duration. The effect on the off-resonance artifacts is clearly visible in the images of Figure 5.9, Figure 5.10 and Figure 5.11. On the left sides of these figures, fully sampled spiral reference images with two, four and eight interleaves are shown (from the top to the bottom). The images with only two interleaves (Figure 5.9, Figure 5.10, and Figure 5.11, upper left corner) clearly suffer from off-resonance artifacts, in particular in regions near air-tissue borders. These effects are greatly reduced by increasing the number of interleaves to four or eight (Figure 5.9, Figure 5.10, and Figure 5.11, center and bottom row). While off-resonance artifacts are decreased with an increased number of interleaves, the acquisition time and therefore the sensitivity to flow and motion are increased. Therefore, the optimal solution for spiral imaging in this case is a single-shot acquisition with the off-resonance behavior of a multi-shot approach. With pMRI we are able to come a step closer to this solution as demonstrated in Figure 5.9, Figure 5.10, and Figure 5.11, where spiral GRAPPA reconstructions with acceleration factors of two, four and eight are shown (right column of both figures). Note that all GRAPPA reconstructions in these figures are single-shot spiral acquisitions. As can be seen in Figure 5.10, artifacts of the direct spiral GRAPPA approach occurs in image blurring. This is clearly visible in the extreme case of acceleration factor of eight reconstructions with only eight coils (see Figure 5.9, bottom row).
A direct comparison between conventional single-shot spiral imaging at 3.0 T and respective eight-fold accelerated GRAPPA undersampled single-shot images from two different slices of a healthy volunteer are shown in Figure 5.12. The long readout duration of 145.5 ms for the conventional single-shot acquisition (left column of Figure 5.12) with an in-plane resolution of 1.25 x 1.25 mm$^2$ results in severe off-resonance artifacts. With an acceleration factor of eight (right column of Figure 5.12), the readout duration is reduced to 18.3 ms and the GRAPPA reconstruction shows significantly improved image quality.

Even though spiral trajectories offer distinct advantages for MRI due to the more efficient use of the gradient capabilities of the MR system and due to the more relaxed pMRI artifact behavior, the application of pMRI techniques to spiral imaging is non-trivial. In general, pMRI reconstructions from undersampled non-Cartesian data require the solution of large linear equation systems, requiring long reconstruction times. Recently presented methods [54]-[58] have been reported to be very time consuming, resulting in reconstruction times for a typical fMRI data set in the order of a day or even longer. With the approach presented in this paper, all GRAPPA reconstruction times were in the range or even less time-consuming than the time needed to perform the gridding procedure. The most time consuming step in the GRAPPA reconstruction is the calculation of the coil weights, which was in general several times longer than the reconstruction of the data itself. In the following two important parameters are discussed, which can be used to optimize image quality and reconstruction time for direct spiral GRAPPA:

1. The kernel size of the GRAPPA reconstruction: It was observed that a 4 x 3 kernel size shows the best performance in terms of image reconstruction time and image quality.
2. Number of segments used for reconstruction: For all examples in this paper 56 segments were used along the azimuthally direction. An additional segmentation along the radial direction can potentially improve the direct GRAPPA reconstruction. However, this also increases the number of reconstruction parameters, and reduces the number of reference data for each segment. This, however, may lead to a reduced quality of the reconstruction parameters and residual artifacts such as spiral fold-over artifacts in the final image.

For multiple repetitions commonly used in dynamic imaging experiments such as fMRI, the acquisition of a complete spiral ACS data set and the determination of the coil weights, the most expensive calculation, have to be performed only once. The calculated coil weights can then be used to reconstruct all images from the time series. To increase the accuracy of the fit over the whole time series, this process could be repeated several times during the acquisition. The time efficiency of the total acquisition would barely be affected by the acquisition of a complete spiral ACS data set every hundredth repetition, for example.

Compared to the method that has been presented recently by Heberlein et al [60]-[62], which is the direct application of the radial GRAPPA approach [59] on spiral data, the direct spiral GRAPPA method [63],[64] described in this chapter includes an optimized GRAPPA reconstruction with an enlarged kernel, interpolation and reordering of the data. These steps allow one to obtain accurate single-shot reconstructions. Furthermore, the high symmetry of the interpolated constant-angular-velocity data makes it possible to improve the fit process, by increasing the number of data points incorporated into a single fit.
5.5 Summary

In this chapter, a new approach for fast spiral pMRI reconstructions has been presented. Compared to previous methods, the reconstruction time is reduced to the same, or even less, time than required for data gridding. The new approach enables high resolution single-shot spiral pMRI applications even for $T_2^*$ weighted fMRI images at high fields. Compared to multi-shot spiral acquisitions, artifacts from physiological effects (e.g. respiration) are reduced in the single-shot spiral GRAPPA approach shown here, which is beneficial for dynamic imaging.
6 Conclusions and Perspectives

Since the first in vivo pMRI implementation, namely SMASH technique in 1997, the field of parallel imaging has greatly expanded to include a variety of techniques, each with different advantages and potential areas of clinical impact. The SENSE technique, introduced in 1998, is the most widespread parallel imaging technique today. Within the last two years, all of the major MRI manufacturers, namely Philips (SENSE), Siemens (mSENSE), GE (ASSET) and Toshiba (SPEEDER), have implemented some type of SENSE algorithm. The only k-space technique that is currently commercially available is the GRAPPA method offered by Siemens. However, regardless of the technique is used, the commercial availability of pMRI means that parallel imaging now has a broad clinical impact beyond high-end research sites. As mentioned earlier, the most evident advantage of using pMRI is the shorter total acquisition time compared to conventional imaging. However, parallel imaging is not without its limitations. Currently, 2D image acquisitions accelerated by a factor of two to three are common for many different clinical applications. This holds true even for the new generation of MR scanners with up to 32 independent receiver channels, which have the potential for much greater acceleration. Higher acceleration factors can be achieved under certain conditions, e.g. when a 3D acquisition is used, exploiting pMRI in two dimensions. As explained in the
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introduction, there are two potential pitfalls which limit the applicability of pMRI with high acceleration rates. First, one has to keep in mind that acceleration with pMRI always incurs an SNR penalty due to the fact that fewer data are actually acquired. An intrinsic loss of at least the square root of the acceleration factor has to be expected for all pMRI reconstruction algorithms.

The second important limitation is due to pMRI reconstruction errors, e.g. residual fold-over artifacts in GRAPPA. This is simply a question of the reliability of the examination. In the introduction, imaging speed was given as the most important consideration for clinical application, besides image contrast. At this point, a third consideration must be added to this list, namely the reliability of pMRI in daily clinical diagnosis. Depending on the imaging sequence and the application, the reliability of all parallel imaging methods is reduced if the acceleration factor reaches a given maximum value.

In this thesis, two new non-Cartesian pMRI methods have been described. Although the GRAPPA methodology was used, all other $k$-space based pMRI techniques can potentially be extended to non-Cartesian acquisitions with the described methods described.

For both methods, it was shown that the synergy of pMRI with non-Cartesian trajectories is beneficial. The direct comparison between the Cartesian and 1D non-Cartesian GRAPPA reconstructions has shown that the 1D non-Cartesian GRAPPA method outperforms conventional Cartesian GRAPPA for high acceleration factors. Residual fold-over artifacts, clearly visible in the Cartesian GRAPPA reconstruction, are significantly reduced in the corresponding 1D non-Cartesian GRAPPA method. In general, there is a trade off between SNR and the reduction of remaining aliasing artifacts. This loss in
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SNR is obviously more than compensated by the reduction of the severe aliasing artifacts in the special case of non-Cartesian pMRI with high acceleration factors presented in this study. The high image quality of the direct spiral GRAPPA acquisitions, even for high acceleration factors, indicates the same.

In conclusion, the non-Cartesian pMRI methods described in this thesis have a more relaxed fold-over artifact behavior, are intrinsically self-calibrating, and make an effective use of the available gradient performance. Those properties directly translate into a superior image quality and in a higher reliability as compared to their Cartesian counterparts. The major hindrance for the use of pMRI in combination with non-Cartesian trajectories has been reconstruction time. This burden can now be overcome, clearing the way for non-Cartesian pMRI in broad clinical use in the near future.
7 Bibliography


8 Summary

Besides image contrast, imaging speed is probably the most important consideration in clinical magnetic resonance imaging (MRI). MR scanners currently operate at the limits of potential imaging speed, due to technical and physiological problems associated with rapidly switched gradient systems. Parallel imaging (parallel MRI or pMRI) is a method which allows one to significantly shorten the acquisition time of MR images without changing the contrast behavior of the underlying MR sequence. The accelerated image acquisition in pMRI is accomplished without relying on more powerful technical equipment or exceeding physiological boundaries. Because of these properties, pMRI is currently employed in many clinical routines, and the number of applications where pMRI can be used to accelerate imaging is increasing. However, there is also growing criticism of parallel imaging in certain applications. The primary reason for this is the intrinsic loss in the SNR due to the accelerated acquisition. In addition, other effects can also lead to a reduced image quality. Due to unavoidable inaccuracies in the pMRI reconstruction process, local and global errors may appear in the final reconstructed image. The local errors are visible as noise enhancement, while the global errors result in the so-called fold-over artifacts. The appearance and strength of these negative effects, and thus the image quality, depend upon different factors, such as the parallel imaging method chosen, specific parameters in the method, the sequence chosen, as well as specific sequence parameters. In general, it is not possible to optimize all of these parameters simultaneously for all applications. A classic example is functional imaging (fMRI), where one cannot employ the robust but comparatively slow FLASH sequence. A sequence with a
much shorter acquisition time is essential to achieve a „snap-shot“ image, where all spurious motion, the so-called physiological noise, is frozen. As a general rule, the fast Echo-Planer sequence (EPI) is employed, although this sequence is sensitive to imaging imperfections. For example, typical EPI artifacts include so-called N/2 ghosts, which can lead to major problems in parallel imaging reconstructions, even when these artifacts appear less pronounced in the non-accelerated, conventional acquired image. There are methods, such as the previously mentioned fMRI EPI sequence, where light ghosting artifacts are tolerable in conventional images. However, the application of parallel imaging in these cases can lead to very pronounced image artifacts, i.e. parallel imaging can amplify errors. On the other hand, there are applications such as abdominal MR or MR angiography, in which parallel imaging does not reconstruct images robustly. Thus, the application of parallel imaging leads to errors. In general, the original euphoria surrounding parallel imaging in the clinic has been dampened by these problems. The reliability of the pMRI methods currently implemented is the main criticism. Furthermore, it has not been possible to significantly increase the maximum achievable acceleration with parallel imaging despite major technical advances. An acceleration factor of two is still standard in clinical routine, although the number of independent receiver channels available on most MR systems (which are a basic requirement for the application of pMRI) has increased by a factor of 3-6 in recent years.

In this work, a novel and elegant method to address this problem has been demonstrated. The idea behind the work is to combine two methods in a synergistic way, namely non-Cartesian acquisition schemes and parallel imaging. The so-called non-Cartesian acquisition schemes have several advantages over standard Cartesian acquisitions, in that they are often faster and less sensitive to physiological noise. In addition, such acquisition schemes

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are very robust against fold-over artifacts even in the case of vast undersampling of \( k \)-space.

There are two reasons for the lower sensitivity of such sequence types to fold-over artifacts. Firstly, fold-over artifacts which are caused by missing or poorly reconstructed data from the central portion of \( k \)-space are very distinct. In most non-Cartesian acquisition schemes a certain part of the central region of \( k \)-space is oversampled, means the sampling rate is higher than the Nyquist rate. Through an oversampling of this area in the center of \( k \)-space, such high-signal artifacts can be avoided. In addition, the fact that the \( k \)-space lines are not equidistant in \( k \)-space means that the FOV is no longer well-defined, and that it changes with the position in \( k \)-space. The positioning of the resulting fold-over artifacts then depends on the size of the FOV. As a result of these non-equidistant lines, the fold-over artifacts are spread over a large area in the image, and appear less strongly than in Cartesian images.

Despite the advantages described above, non-Cartesian acquisition schemes are not commonly employed in clinical routines. A reason for that is the complicated reconstruction techniques which are required to convert the non-Cartesian data to a Cartesian grid before the fast Fourier transformation can be employed to arrive at the final MR image. Another reason is that Cartesian acquisitions are routinely accelerated with parallel imaging, which is not applicable for non-Cartesian MR acquisitions due to the long reconstruction times. This negates the speed advantage of non-Cartesian acquisition methods.

Through the development of the methods presented in this thesis, reconstruction times for accelerated non-Cartesian acquisitions using parallel imaging now approach those of Cartesian images. In this work, the reliability of such methods has been demonstrated. In addition, it has been shown that higher acceleration factors can be achieved with such techniques than possible with Cartesian imaging.
These properties of the techniques presented here lead the way for an implementation of such methods on MR scanners, and thus also offer the possibility for their use in clinical routine. This will lead to shorter examination times for patients as well as more reliable diagnoses.
Zusammenfassung

noch ein Beschleunigungsfaktor von zwei, obwohl sich die Anzahl der unabhängigen Empfangskanäle eines MR-Systems (eine Grundvoraussetzung für die Verwendung der pMRT) in den letzten Jahren um einen Faktor 3-6 erhöht hat.


Es gibt zwei Gründe für die geringere Empfindlichkeit gegenüber Faltungsartefakten bei diesen Sequenztypen. Faltungsartefakte, welche durch fehlende oder fehlerhaft rekonstruierte Daten aus dem zentralen \( k \)-Raumbereich resultieren, sind besonders stark ausgeprägt. Bei den meisten nicht-kartesischen Aufnahmeverfahren wird ein Teil des zentralen \( k \)-Raumes überabgetastet, d.h. die Abtastrate ist größer als die Nyquist-Abtastrate. Durch das Überabtasten dieses Bereichs im \( k \)-Raumzentrum werden signalstarke Faltungsartefakte von vornherein vermieden. Des Weiteren ist durch die nicht äquidistante Schrittweite im \( k \)-Raum das Sichtfeld nicht länger wohl definiert und ändert sich mit der \( k \)-Raumposition. Das Erscheinungsbild der Faltungsartefakte hängt jedoch von der Größe des Sichtfeldes ab. Als ein Ergebnis der nicht äquidistanten Schrittweite werden Faltungsartefakte über einen weiten Bereich verschmiert und erscheinen dadurch weniger stark ausgeprägt.


10 Publications

Papers


Robin M. Heidemann, Mark A. Griswold, Mathias Müller, Felix Breuer, Martin Blaimer, Berthold Kiefer, Melanie Schmitt, Peter M. Jakob. Möglichkeiten und Grenzen der Parallelen MRT im


Patents


Invited Talks


11 Curriculum Vitae

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Rossdorf, August 13\textsuperscript{th} 2007

(Robin Heidemann)
12 Acknowledgments

My MR life began the moment I entered the office of Peter Jakob to ask for a topic for my diploma thesis. It was a great decision to start my diploma thesis on the topic of parallel imaging with Peter Jakob as supervisor. Only a few months later, a guy from the United States came to our lab to stay for a year or so. It was a real pleasure to share an office with Mark Griswold for about 6 years. The next highlight was the arrival of Mark’s old professor from Illinois, who also ended up sitting in our office. The stay of Andrew Webb was a real highlight of my Doctoral work, and it turned out that he is not an old professor.

I owe a big “thank you” to these three people, who have influenced my MR life more than anybody else. If there is anything wrong or poorly explained in this thesis, it is only because I have not listened carefully enough to their advice.

Further, I wish to thank Professor Axel Haase for the opportunity to do my diploma and my PhD thesis in his department, and for the unforgettable team events.

Nicole Seiberlich and Andrew deserve a lot of thanks for correcting most of the more confusing Fränghlish expressions in this manuscript.

A big thanks goes to my former roommates Thomas Neuberger, David Balla, Mathias Nahrendorf, and Michael Szimtenings.
It was a pleasure to work in the parallel imaging team together with Peter, Mark, David, Nicole, Martin Blaimer, Felix Breuer and Mathias Mueller. It was always helpful for me to discuss all kind of things with you.

The constant support of Siemens Medical Solutions, namely Gunnar Krueger, Mathias Nittka, Stephan Kannengiesser, Vladimir Jellus and Berthold Kiefer is the main reason for all the good images in this thesis. Through the collaboration with Siemens, I came into contact with the following people, who I would also like to thank:

Professor Paul Parizel and Dr. Oezkan Oezsarlan from the University of Antwerp for the fruitful cooperation during the work on my first review paper.

Professor Larry Wald and Dr. Graham Wiggins from the MGH in Boston for the cooperation on the 32 channel spiral GRAPPA results; the coil is a piece of art.

I also wish to thank my new roommates at Siemens, Josef Pfeuffer and Stefan Huwer for everything they have done for me.

I have probably forgotten to mention several people in this acknowledgment who also deserve recognition. I am sorry for this!

Finally, at the very end of this thesis... I am grateful to my wife Christine, my daughter Lea and my son Jannes, simply for being here.
EHRENWÖRTLICHE ERKLÄRUNG

gemäß §5 Abs. 2 Ziff. 2 und 5
der Promotionsordnung der
Fakultät für Physik und Astronomie der
Universität Würzburg

Hiermit erkläre ich ehrenwörtlich, dass ich die Dissertation selbstständig
und ohne Hilfe eines Promotionsberaters angefertigt und keine anderen
als die angegebenen Quellen und Hilfsmittel benutzt habe.

Die Dissertation wurde bisher weder vollständig noch teilweise einer
anderen Hochschule mit dem Ziel einen akademischen Grad zu
erwerben vorgelegt.

Im Mai 2000 wurde mir von der Universität Würzburg der akademische
Grad „Diplom-Physiker“ verliehen. Weitere akademische Grade habe
ich weder erworben noch versucht zu erwerben.

Rossdorf, August 13\textsuperscript{th} 2007

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(Robin Heidemann)